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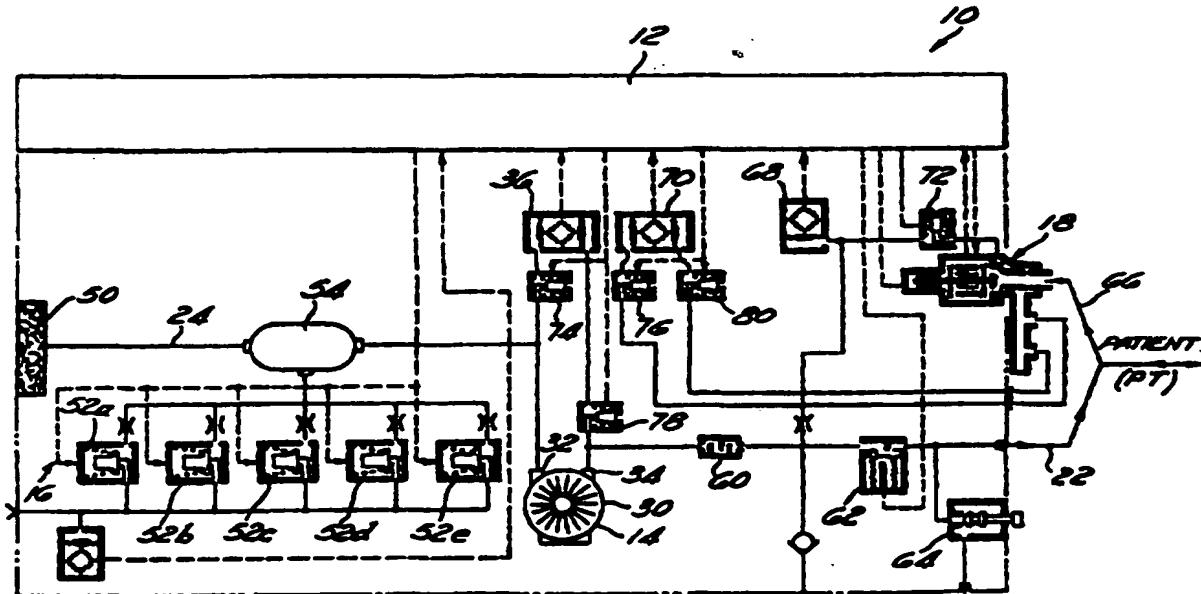
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(71) Applicant: BIRD PRODUCTS CORPORATION [US/US]; 1100 Bird Center Drive, Palm Springs, CA 92262 (US).			
(72) Inventors: DEVRIES, Douglas, F.; 10345 Walnut Grove Court, Yucaipa, CA 92399 (US). CEGIELSKI, Michael, J.; 2404 Temescal Avenue, Norco, CA 91760 (US). GRAVES, Warner, V., Jr.; 41297 Plumrose Street, Hemet, CA 92544 (US). WILLIAMS, Malcolm, R.; 3824 Calle Ariana, San Clemente, CA 92672 (US). HOLMES, Michael, B.; 11031 Campbell Avenue, Riverside, CA 92505 (US).			
(74) Agents: STETINA, Kit, M. et al.; Stetina Brunda & Buyan, Suite 401, 24221 Calle de la Louisa, Laguna Hills, CA 92653 (US).			

(54) Title: PORTABLE DRAG COMPRESSOR POWERED MECHANICAL VENTILATOR



(57) Abstract

A ventilator system (10) comprising a rotary drag compressor (30), an exhalation valve (18), gas blender (16) with multiple solenoid valves (52), a differential pressure transducer (36) and data look-up control system, where the ventilator system is portable and battery powered.

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PORTABLE DRAG COMPRESSOR POWERED MECHANICAL VENTILATOR

Field of the Invention

The present invention pertains generally to medical equipment and more particularly to a compressor powered mechanical ventilator device for delivering respiratory ventilation to a mammalian patient.

Background of the Invention

A. Principles of Mechanical Ventilation

In many clinical settings mechanical ventilators are used to facilitate the respiratory flow of gas into and out of the lungs of patients who are sick, injured or anesthetized.

In general, mechanical ventilators provide a repetitive cycling of ventilatory flow, each such repetitive cycle being separated into two phases--an inspiratory phase followed by an expiratory phase.

The inspiratory phase of the ventilator cycle is characterized by the movement of positive-pressure inspiratory flow of gas through the ventilator circuit and into the lungs of the patient. The expiratory phase of the ventilatory cycle is characterized by cessation of the positive pressure inspiratory flow long enough to allow lung deflation to occur. The exhaled gas is vented from the ventilator circuit, typically through an exhalation valve. In patient whose lungs and thoracic musculature exhibit normal compliance, the act of exhalation is usually permitted to occur spontaneously without mechanical assistance from the ventilator.

It is sometimes desirable to control the airway pressure during exhalation to maintain a predetermined amount of positive back pressure during all, or a portion of, the respiratory cycle. Such techniques are often utilized to treat impairments of lung capacity due to pulmonary atelectasis or other factors.

The mechanical ventilators of the prior art have been grouped under various classification schemes, based on various criteria. In general, mechanical ventilators

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may be grouped or classified according to the parameter(s) which are utilized for a) triggering, b) limiting and c) terminating (e.g., cycling) the inspiratory phase of the ventilator cycle.

5 **"Triggering"** is the action that initiates the inspiratory phase of the ventilator cycle. The initiation of the inspiratory phase may be triggered by the ventilator or the patient. The variables and/or parameters which are utilized to trigger the beginning of
10 the inspiratory phase include: time (i.e., respiratory rate), the commencement of spontaneous inhalation by the patient and/or combinations thereof.

15 **"Limiting"** of the inspiratory phase refers to the manner in which the inspiratory gas flow is maintained within prescribed ranges to optimize the ventilation of the patient's lungs. The limiting variables and/or parameters are typically controlled by the ventilator, but may change as a result of patient effort and/or physiologic variables such as lung compliance and airway
20 resistance. The variables and/or parameters which are utilized for limiting the inspiratory phase include flow rate, airway pressure and delivered volume.

25 **"Terminating"** or **"cycling"** of the inspiratory phase of the ventilator cycle refers to the point at which the inspiratory flow is stopped and the ventilator and/or patient are permitted to "cycle" into the expiratory phase. Depending on the ventilator control settings, the termination of the inspiratory phase may be brought about by the ventilator or the patient. The variables and/or
30 parameters which are utilized to terminate the inspiratory phase include: time; peak airway pressure; and/or tidal volume (V_t).

B. Mechanical Ventilation Modes Utilized In Modern Clinical Practice

35 In addition Mechanical ventilators are utilized to deliver various "modes" of mechanical ventilation, the particular mode of ventilation being selected or

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prescribed based on the clinical condition of the patient and the overall objective (i.e., long term ventilation, short term ventilation, weaning from ventilator, etc...) of the mechanical ventilation.

5

I. Ventilation Modes:

i. **Intermittent Mandatory Ventilation (IMV)**

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Intermittent Mandatory Ventilation is a ventilation mode wherein a spontaneously breathing patient receives intermittent mechanical inflation supplied asynchronously by the ventilator.

ii. **Synchronized Intermittent Mandatory Ventilation (SMIV)**

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Synchronized Intermittent Mandatory Ventilation is a ventilation mode wherein a spontaneously breathing patient receives occasional mandatory ventilatory breaths. Mandatory ventilator breaths are synchronized with the patient's spontaneous inspiratory efforts.

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iii. **Controlled Mechanical Ventilation (CMV)**

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Controlled Mechanical Ventilation (CMV) is a ventilation mode wherein mechanical breaths are delivered to the patient at time intervals which are unaffected by patient efforts. Controlled Mechanical Ventilation is typically utilized in patients who are not breathing spontaneously.

iv. **Assist/Control Ventilation (A/C)**

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Assist/Control Ventilation (A/C) is a ventilation mode wherein the patient is able to volitionally alter the frequency of mandatory ventilator breaths received, but can not alter the flow and title volume (V_t) of each ventilator breath received. Controlled, mandatory breaths are initiated by the ventilator based on the set breath rate. In addition, the patient can demand and trigger

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an assist breath. After successful triggering of an assist breath, the exhalation valve is closed and gas is delivered to the patient to satisfy the preset tidal volume, peak flow and wave form.

5 C. Breath Types Utilized in Modern Clinical Practice

Breath types are typically classified according to the particular functions which control:

10 a) triggering;

 b) limiting; and

 c) cycling of each breath delivered by the mechanical ventilator, as described and defined hereabove.

15 Typical breath types and ventilator parameters utilized in modern clinical practice include the following:

 i. **Machine-Cycled--Mandatory Breath**

20 A machine-cycled, mandatory breath is a breath that is triggered, limited and cycled by the ventilator.

 ii. **Machine-Cycled--Assist Breath**

 A machine cycled assist breath is a breath that is triggered by the patient, but is limited and cycled by the ventilator.

25 iii. **Patient-Cycled--Supported Breath**

 A patient-cycled, supported breath is a breath that is triggered by the patient, limited by the ventilator, and cycled by the patient.

 iv. **Patient-Cycled--Spontaneous Breath**

30 A patient-cycled spontaneous breath is a breath that is triggered, limited and cycled by the patient. While patient effort limits the flow, and hence the inspiratory volume of the breath, the ventilator may also limit the breath by providing a flow that is too low to maintain a constant pressure in the face of patient inspiratory demand.

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v. Volume-Controlled Mandatory Breaths

Volume-controlled breaths are machine-triggered mandatory breaths. The inspiratory phase is initiated by the ventilator based on a preset breath rate. The inspiratory phase is ended, and the expiratory phase begun, when the breath delivery is determined to be complete based on a preset tidal volume, peak flow and wave form setting. The ventilator remains in expiratory phase until the next inspiratory phase begins.

vi. Volume-Controlled--Assist Breaths

Volume-controlled breaths are machine cycled supported breaths that are initiated by the patient. Volume-controlled assist breaths may be initiated only when the "assist window" is open. The "assist window" is the interval or time during which the ventilator is programmed to monitor inspiratory flow for the purpose of detecting patient inspiratory effort. When a ventilator breath is triggered, the inspiratory phase of such breath will continue until a preset tidal volume peak flow and wave form have been achieved. Thereafter, the exhalation valve is open to permit the expiratory phase to occur. The ventilator remains in the expiratory phase until the next patient-triggered breath, or the next mandatory inspiratory phase, begins.

vii. Pressure-Controlled Breaths

Pressure-Controlled breaths are delivered by the ventilator using pressure as the key variable for limiting of the inspiratory phase. During pressure control, both the target pressure and the inspiratory time are set, and the tidal volume delivered by the ventilator is a function of these pressure and time settings. The actual tidal volume delivered in each pressure-controlled breath is strongly influenced by patient physiology.

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viii. Pressure Support Breaths

Pressure support breaths are triggered by the patient, limited by the ventilator, and cycled by the patient. Thus, each breath is triggered by patient inspiratory effort, but once such triggering occurs the ventilator will assure that a predetermined airway pressure is maintained through the inspiratory phase. The inspiratory phase ends, and the expiratory phase commences, when the patients inspiratory flow has diminished to a preset baseline level.

ix. Sigh Breaths

A sigh breath is a machine-triggered and cycled, volume-controlled, mandatory breath, typically equal to 1.5 times the current tidal volume setting. The inspiratory phase of each sigh breath delivers a preset tidal volume and peak flow. The duration of the inspiratory phase of each sigh breath is limited to a maximum time period, typically 5.5 seconds. The ventilator may be set to deliver a sigh function automatically after a certain number of breaths or a certain time interval (typically 100 breaths for every 7 minutes), which ever interval is shorter. The sigh breath function it may be utilized during control, assist and SIMV modes of operation, and is typically disabled or not utilized in conjunction with pressure controlled breath types or continuous positive air way pressure (CPAP).

x. Proportional Assist Ventilation (PAV)

Proportional Assist Ventilation (PAV) is a type of ventilator breath wherein the ventilator simply amplifies the spontaneous inspiratory effort of the patient, while allowing the patient to remain in complete control of the tidal volume, time duration and flow pattern of each breath received.

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xi. Volume Assured Pressure Support (VAPS)

Volume Assured Pressure Support (VAPS) is a type of ventilator breath wherein breath initiation and delivery is similar to a pressure support breath. Additionally, the ventilator is programmed to ensure that a preselected tidal volume (V_t) is delivered during such spontaneously initiated breath.

D. Oxygen Enrichment Of The Inspiratory Flow

It is sometimes desirable for mechanical ventilators to be equipped with an oxygen-air mixing apparatus for oxygen enrichment of the inspiratory flow. Normal room air has an oxygen content (FiO_2) of 21%. In clinical practice, it is often times desirable to ventilate patients with oxygen FiO_2 from 21% to 100%. Thus, it is desirable for mechanical ventilators to incorporate systems for blending specific amounts of oxygen with ambient air to provide a prescribed oxygen-enriched FiO_2 . Typically, volume-cycle ventilators which utilize a volume displacement apparatus have incorporated oxygen mixing mechanisms whereby compressed oxygen is combined with ambient air to produce the selected FiO_2 as both gases are drawn into the displacement chamber during the expiratory phase of the ventilator cycle. Nonbellows-type volume-cycled ventilators have incorporated other air-oxygen blending systems for mixing the desired relative volumes of oxygen and air, and for delivering such oxygen-air mixture through the inspirations circuitry of the ventilator.

E. Regulation/Control Of Expiratory Pressure

The prior art has included separately controllable exhalation valves which may be preset to exert desired patterns or amounts of expiratory back pressure, when such back pressure is desired to prevent atelectasis or to otherwise improve the ventilation of the patient.

The following are examples of expiratory pressure modes which are frequently utilized in clinical practice:

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i. Continuous Positive Airway Pressure (CPAP)

Continuous Positive Airway Pressure (CPAP) is employed during periods of spontaneous breathing by the patient. This mode of ventilation is characterized by the maintenance of a continuously positive airway pressure during both the inspiratory phase, and the expiratory phase, of the patient's spontaneous respiration cycle.

ii. Positive End Expiratory Pressure (PEEP)

In Positive End Expiratory Pressure a predetermined level of positive pressure is maintained in the airway at the end of the expiratory phase of the cycle. Typically, this is accomplished by controlling the exhalation valve so that the exhalation valve may open only until the circuit pressure has decreased to a preselected positive level, at which point the expiration valve closes again to maintain the preselected positive end expiratory pressure (PEEP).

F. Portable Ventilators of the Prior Art

The prior art has included some non-complex portable ventilators which have inherent limitations as to the number and type of variables and/or parameters which may be utilized to trigger, limit and/or terminate the ventilator cycle. Although such non-complex ventilators of the prior art are often sufficiently power efficient and small enough for portable use, their functional limitations typically render them unsuitable for long term ventilation or delivery of complex ventilation modes and or breath types.

The prior art has also included non-portable, complex microprocessor controlled ventilators of the type commonly used in hospital intensive care units. Such ventilators typically incorporate a microcomputer controller which is capable of being programmed to

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utilize various different variables and/or parameters for triggering, limiting and terminating the inspiratory phase of the ventilator cycle. Complex ventilators of this type are typically capable of delivering many
5 different ventilation modes and or breath types and are selectively operable in various volume-cycled, pressure cycled or time-cycled modes. However, these complex ventilators of the prior art have typically been too large in size, and too power inefficient, for battery-driven portable use. As a result of these factors, most
10 of the complex micro-processor controlled ventilators of the prior art are feasible for use only in hospital critical care units.

As is well known there exist numerous settings,
15 outside of hospital critical care units, where patients could benefit from the availability of a small, battery powered, complex microprocessor controlled mechanical ventilator capable of delivering extended modes of ventilation. For example, critically ill patients
20 sometimes require transport outside of the hospital in various transport vehicles, such as ambulances and helicopters. Also, critical care patients are sometimes transiently moved, within the hospital, from the critical care unit to various special procedure areas (e.g.,
25 radiology department, emergency room, catheterization lab etc.,) where they may undergo diagnostic or therapeutic procedures not available in the critical care unit. Additionally, patients who require long term ventilation are not always candidates for admission to acute care
30 hospital critical care units or may be discharged to step-down units or extended care facilities. Also, some non-hospitalized patients may require continuous or intermittent ventilatory support. Many of these patients could benefit from the use of complex microprocessor
35 controlled ventilators, but may be unable to obtain such benefit due to the non-feasibility of employing such

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ventilators outside of the hospital-critical care unit environment.

In view of the foregoing limitations on the usability of prior art complex microprocessor controlled 5 volume-cycled ventilators, there exists a substantial need in the art for the development of a portable, highly efficient, ventilator capable of programmed delivery of various modern ventilatory modes and breath types, while also being capable of use outside of the hospital 10 critical care unit environment, such as in transport vehicles, extended care facilities and patients homes, etc.

United States Patent No. 4,493,614 (Chu et al.) entitled "PUMP FOR A PORTABLE VENTILATOR" describes a 15 reciprocating piston pump which is purportedly usable in a portable ventilator operable on only internal or external battery power.

United States Patent No. 4,957,107 (Sipin) entitled "GAS DELIVERY MEANS" describes a rotating drag compressor 20 gas delivery system which is ostensibly small enough to be utilized in a portable ventilator. The system described in U.S. Patent No. 4,957,107 utilizes a high speed rotary compressor which delivers a substantially constant flow of compressed gas. The rotary compressor 25 does not accelerate and decelerate at the beginning and end of each inspiratory phase of the ventilator cycle. Rather, the rotating compressor runs continuously, and a diverter valve is utilized to alternately direct the outflow of the compressor a) into the patients lungs 30 during the inspiratory phase of the ventilation cycle, and b) through an exhaust pathway during the expiratory phase of the ventilation cycle.

Thus, there remains a substantial need for the development of an improved portable mechanical ventilator 35 which incorporates the following features:

A. Capable of operating for extended periods (i.e., at least 2½ hours) using a

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single portable battery or battery pack as the sole power source;

5 B. Programmable for use in various different ventilatory modes, such as the above-described IMV, SMV, CMV, PAV, A/C and VPAS.

C. Usable to ventilate non-intubated mask patients as well as intubated patients.

10 D. Oxygen blending capability for delivering oxygen-enriched inspiratory flow.

E. Capable of providing controlled exhalation back pressure for CPAP or PEEP.

F. Portable, e.g., less than 30 lbs.

Summary of the Invention

15 The present invention specifically addresses the above referenced deficiencies and needs of the prior art by providing comprises a mechanical ventilator device which incorporates a rotary compressor for delivering intermittent inspiratory gas flow by repeatedly accelerating and decelerating the compression rotor at the beginning and end of each inspiratory phase. Prior to commencement of each inspiratory ventilation phase, the rotary compressor is stopped, or rotated at a basal rotational speed. Upon commencement of an inspiratory phase, the rotary compressor is accelerated to a greater velocity for delivering the desired inspiratory gas flow. At the end of each inspiratory phase, the rotational velocity of the compressor is decelerated to the basal velocity, or is stopped until commencement of the next 25 inspiratory ventilation phase. A programmable controller is preferably incorporated to control the timing and rotational velocity of the compressor. Additionally, the controller may be programmed to cause the compressor to operate in various modes of ventilation, and various 30 breath types, as employed in modern clinical practice.

35 Further in accordance with the present invention, there is provided an oxygen blending apparatus which may

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be utilized optionally with the rotatable compressor ventilation device of the present invention. The oxygen blending apparatus of the present invention comprises a series of valves having flow restricting orifices of
5 varying size. The valves are individually opened and closed to provide a desired oxygen enrichment of the inspiratory gas flow. The oxygen blending apparatus of the present invention may be controlled by a programmable controller associated with, or separate from, the
10 ventilator controller.

Still further in accordance with the invention, there is provided an exhalation valve apparatus comprising a housing which defines an expiratory flow path therethrough and a valving system for controlling
15 the airway pressure during the expiratory phase of the ventilation cycle. A pressure transducer monitors airway pressure during exhalation the output of which is used by the controller to adjust the valving system to maintain desired airway pressure.

20 In addition the present invention utilizes an exhalation flow transducer to accurately measure patient exhalation flow which may be utilized for determination of exhaled volume and desired triggering of inspiratory flow. In the preferred embodiment, the exhalation flow
25 transducer is integrally formed with the exhalation valve, however, those skilled in the art will recognize that the same can be a separate component insertable into the system. To insure transducer performance accuracy, in the preferred embodiment, the particular operational
30 characteristics of each flow transducer are stored within a memory device preferably a radio-frequency transponder mounted within the exhalation valve to transmit the specific calibration information for the exhalation flow transducer to the controller. Further, the particular
35 construction and mounting of the flow transducer within the exhalation valve is specifically designed to minimize fabrication inaccuracies.

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Further objects and advantages of the invention will become apparent to those skilled in the art upon reading and understanding of the following detailed description of preferred embodiments, and upon consideration of the accompanying drawings.

Brief Description of the Drawings

Figure 1 is a basic schematic diagram of a preferred ventilator system of the present invention incorporating, a) a rotary compressor ventilator device, b) an optional air-oxygen blending apparatus; and c) a controllable exhalation valve, and d) a programmable controller or central processing unit (CPU) which is operative to control and coordinate the functioning of the ventilator, oxygen blending apparatus and exhalation valve.

Figure 2 is a detailed schematic diagram of a ventilator system of the present invention.

Figure 3 is a front view of the control panel of a preferred ventilator system of the present invention.

Figure 4 is a perspective view of a preferred drag compressor apparatus which may be incorporated into the ventilator system of the present invention.

Figure 5 is a longitudinal sectional view through line 5-5 of Figure 4.

Figure 6 is an enlarged view of a segment of Figure 5.

Figure 7 is an enlarged view of a segment of Figure 6.

Figure 8 is an elevational view of a preferred drag compressor component of a mechanical ventilator device of the present invention.

Figure 9 is a perspective view of the drag compressor component of Figure 8.

Figure 10 is an enlarged view of a segment of Figure 9.

Figure 11a is a longitudinal sectional view of a preferred exhalation valve of the present invention.

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Figure 11b is a perspective view of the preferred spider bobbin component of the exhalation valve shown in Figure 11a.

5 Figure 11c is an exploded perspective view of a portion of the exhalation valve of Figure 11a.

Figure 11d is a perspective view of a portion of the exhalation valve shown in Figure 11c.

10 Figure 11e is an exploded perspective view of the preferred flow restricting flapper component of the exhalation valve shown in Figures 11a-11d.

Figure 12 is a graphic example of flow vs. speed vs. pressure data generated for a preferred exhalation valve of the present invention, accompanied by an exhalation valve characterization algorithm computed therefrom.

15 **Detailed Description of the Preferred Embodiment**

The following detailed description and the accompanying drawings are provided for purposes of describing and illustrating a presently preferred embodiment of the invention and are not intended to 20 describe all embodiments in which the invention may be reduced to practice. Accordingly, the following detailed description and the accompanying drawings are not to be construed as limitations on the scope of the appended claims.

25 **A. General Description of the Preferred Ventilator System**

With reference to Figures 1-2, the mechanical ventilation system 10 of the present invention generally comprises a) a programmable microprocessor controller 12, 30 b) a ventilator device 14, c) an optional oxygen blending apparatus 16 and d) an exhalation valve apparatus 18. Which is preferably implemented as a portable, battery powered system.

The ventilator device 14 incorporates a rotating 35 drag compressor 30 which is driven by an electric motor 102. In response to control signals received from controller 12, a bladed rotor within the compressor 30

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will undergo rotation for specifically controlled periods of time and/or, within specifically controlled parameters, so as to provide inspiratory gas flow through line 22 to the patient PT.

5 The controller 12 comprises a programmable microprocessor which is electrically interfaced a) to the ventilator device 14 by way of control line 13, b) to the optional oxygen blending apparatus 16 by way of control line 17, and c) to the exhalation valve 18 by way of 10 control line 19 and also by RF communication between flow transducer transponder (21) and transmitter/receiver (23). Preferably incorporated into the exhalation valve 18 as will be described in more detail infra.

15 The controller 12 is preferably programmed to utilize selected parameters (e.g., time, flow rate, tidal volume (V_t), airway pressure, spontaneous breath initiation, etc.) for triggering, limiting and cycling the inspiratory flow in accordance with the selected ventilatory mode or breath type.

20 At the end of each inspiratory flow cycle, the patient PT is permitted to exhale through exhalation valve 18. The flow rate or pressure of the expiratory flow through exhalation valve 18 is controlled by varying the degree of flow restriction within the exhalation valve 18, in response to control signals received through line 19 from controller 12. This enables the exhalation valve 18 to be utilized to create a selected expiratory back pressure (e.g., CPAP, PEEP).

30 Optional oxygen blending apparatus 16 may be utilized to enrich the oxygen content of the inspiratory gas flow provided by the drag compressor ventilator device 14. The preferred oxygen blending apparatus 16 comprises a plurality of (preferably five (5)) solenoid valves 52, each having a specific sized flow restricting orifice. The solenoid valves 52 are arranged in parallel between an oxygen inflow manifold 26 and an oxygen outflow manifold 28. The controller 12 is programmed to

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open and close the individual solenoid valves 52 for specific periods of time so as to provide a metered flow of oxygen through oxygen outflow manifold 28 and into accumulator 54. Ambient air is drawn through conduit 24 5 and filter 50, into accumulator 54, where the ambient air combines with the metered inflow of oxygen to provide an oxygen-enriched inspiratory flow containing a prescribed oxygen concentration (FIO_2).

The presently preferred embodiment of the system 10 10 will operate when supplied with voltage input within the range of 85-264 VAC at 50/60 Hz.

An AC power cord is preferably connectable to the system 10 to provide AC power input.

Additionally, the system 10 preferably includes an 15 internal battery capable of providing at least 15 minutes, and preferably 30 minutes, of operation. During internal battery operation, some non-essential displays may be dimmed or disabled by the controller 12. The internal battery is preferably capable of being recharged 20 by AC power input provided through the AC power cable, or by a separate battery charger. The internal battery is preferably capable of being fully charged, from a no charged state, within 24 hours. The internal battery charge light 306 shown on the panel of the preferred 25 controller 12a may additionally flash if desired during charging of the internal battery.

Also, the system may include an external battery or battery set capable of providing at least 2 hours of operation, and preferably capable of providing 4 to 8 30 hours of operation. During external battery use, some non-essential displays may be dimmed or disabled by the controller 12. The battery or battery set is preferably capable of being recharged by delivery of AC power through the AC power cable, or by a separate battery 35 charger. It is preferable that the external battery or battery set be capable of being fully charged, from a no charged state within 24 to 48 hours. The external

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battery charge light 310 on the panel of the preferred controller 12a may additionally flash if desired during charging of the external battery or battery set.

B. The Preferred Controller Apparatus

5 It will be appreciated that the controller 12 of the ventilator system 10 of the present invention will vary in complexity, depending on the specific capabilities of the system 10, and whether or not the optional oxygen blending apparatus 16 is incorporated.

10 Figure 3 shows the control panel of a preferred controller apparatus 12a which is usable in connection with a relatively complex embodiment of the ventilatory system 10, incorporating the optional oxygen blending apparatus 16.

15 **CONTROLS SETTINGS AND DISPLAYS**

The specific control settings and displays which are included in the preferred controller 12a, and the ways in which the preferred controller 12a receives and utilizes operator input of specific control settings, are 20 described herebelow:

1. **Standby-Off Control**

25 The ventilator system 10 incorporates a stand by/off switch (not shown) which turns the main power on or off. A group of indicator lights 300 are provided on the face panel of the controller 12a, and are more fully described herebelow under the heading "monitors". In general, the panel indicator lights include an "on" indicator 302 which becomes illuminated when the ventilator is turned on. An AC power low/fail indicator light 304 activates when the AC power cord is present and the voltage is out of a specified operating range. Upon sensing low or faulty AC power, the controller 12a will automatically switch the ventilator 14 to internal battery power. The ventilator will continue to operate on internal battery power until such time as 30 power in the internal battery reaches a minimum 35

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level. When the power in the internal battery reaches a minimum level, the controller 12a will cause the internal battery light and/or audible alarm 308 to signal that the internal battery is near depletion.

A separate external battery light and/or audible alarm 312 is also provided. The external battery light and/or audible alarm will activate when the external battery is in use, and has a battery voltage which is out of the acceptable operation range. During this condition, the controller 12a will cause all nonessential displays and indicators to shut down.

When AC power is connected to the ventilator 14, but the ventilator is turned off, any internal or external batteries connected to the ventilator will be charged by the incoming AC current. Internal battery charge indicator light 306 and external battery charge indicator light 306 and external battery charged indicator light 310 are provided, and will blink or otherwise indicate charging of the batteries when such condition exists.

2. Mode Select

A mode select module 320 incorporates plural, preferably five (5) mode select buttons 322, 324, 326, 328, 330. Mode select button 322 sets the system 10 for Assist Control (a/c). Mode select button 324 sets the system 10 for Synchronized Intermittent Mandatory Ventilation (SIV). Mode select button 326 sets the system for Continuous Positive Airway Pressure (CPAP). Spare mode select buttons 328, 330 are provided to permit the controller 12a to be programmed for additional specific ventilation modes such as volume assured pressure support (VAPS) or proportional assist ventilation. When the controller is programmed for

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additional specific ventilation modes, select buttons 328, 330 may be correspondingly labeled and utilized to set the ventilator 14 to deliver such subsequently programmed ventilation modes.

5 3. Tidal Volume

A digital tidal volume display 332, with corresponding tidal volume setting button 332a are provided. When tidal volume setting button 332a is depressed, value setting knob 300 may be utilized to dial in a selected tidal volume. The tidal volume display 332 will then provide a digital display of the currently selected tidal volume value.

10 The typical range of setable tidal volumes is 25ml - 2000ml.

15 4. Breath Rate

A digital breath rate display 334, with corresponding breath rate setting button 334a is provided. When breath rate setting button 334a is depressed, value setting knob 300 may be utilized to dial in the desired breath rate. Breath rate display 334 will thereafter display the currently selected breath rate.

20 The typical range of selectable breath rates is 0 to 80 breaths per minute.

25 5. Peak Flow

A digital peak flow display 336, and corresponding peak flow setting button 336a are provided. When peak flow setting button 336a is depressed, value setting knob 300 may be utilized to dial in the desired peak flow. The peak flow display 336 will, thereafter, provide a digital display of the currently selected peak flow.

30 The typical range of peak flow settings is 10 to 140 liters per minute.

35 6. Flow Sensitivity

A flow sensitivity digital display 338, and corresponding flow sensitivity setting button 338a

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are provided. When flow sensitivity setting button 338a is depressed, value setting knob 300 may be utilized to dial in the desired flow sensitivity setting. The flow sensitivity setting display 338 will, thereafter, provide a digital display of the currently selected flow sensitivity setting.

The flow sensitivity setting determines the trigger level for initiation of volume and pressure-controlled assist breaths or pressure support breaths. The initiation of volitional inspiratory effort by the patient creates a change in airway flow as determined by: (turbine bias flow) - (exhalation flow) = patient flow. Triggering occurs when the patient airway flow exceeds the sensitivity setting. The typical range of selectable flow sensitivity settings is from one to ten liters per minute, or off.

Optionally, a fail safe feature may be incorporated whereby, if the patients flow demand does not exceed the flow sensitivity setting, but the airway pressure drops more than 5 cmH₂O below the set PEEP level, and inspiratory cycle will be initiated and a breath will be delivered based on current mode and control settings.

7. PEEP/CPAP

A PEEP/CPAP digital display 340, with corresponding PEEP/CPAP setting button 340a are provided. When PEEP/CPAP setting button 340a is depressed, the value setting knob 300 may be utilized to dial in the desired PEEP/CPAP setting.

The current PEEP/CPAP setting sets the level of pressure in the patient circuit that is maintained between the end of inspiration and the start of the next inspiration. It is also known as the "baseline" pressure.

The preferred range of PEEP/CPAP setting is 0 to 50 cmH₂O.

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8. Pressure Support

5 A pressure support digital display 342, and corresponding pressure support setting button 342a, are provided. When pressure support setting button 142a is depressed, value setting knob 300 may be utilized to dial in the desired pressure support setting.

10 The pressure support setting determines the inspiratory patient circuit pressure during a pressure support breath. This control sets the pressure support level above the baseline setting established by the PEEP/CPAP setting. The total delivered pressure equals the PEEP or CPAP value + pressure support.

15 The typical range of pressure support settings is from 1 to 60 centimeters of water (cmH₂O), or off.

9. FiO₂(%O₂)

20 An FiO₂ digital display 348, and corresponding FiO₂ setting button 348a, are provided. When the FiO₂ setting button 348a is depressed, the value setting knob 300 may be utilized to dial in the desired fractional percentage of oxygen in the air/oxygen gas mixture that is delivered to the patient PT and used for the bias flow. In response to the FiO₂ setting, the controller 12 will issue control signals to the oxygen blending apparatus 16 to effect the preset FiO₂.

25 The preferred range of setable FiO₂ is between 0.21 and 1.0 (i.e., 21-100 percent oxygen)

10. Pressure Control (Optional)

30 A pressure control digital display 350, and corresponding pressure control setting button 350a are provided. When the pressure control setting button 350a is depressed, the value setting knob 300 may be utilized to dial in the desired pressure control value.

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The pressure control setting enables the system
10 to be utilized for pressure control ventilation,
and determines the inspiratory pressure level during
delivery of each pressure control breath. The
5 pressure control setting sets the pressure level
above any PEEP.

It is preferable that the range of possible
pressure control settings be from 1 to 100 cmH₂O.

11. Inspiratory Time (Optional)

10 An optional inspiratory time digital display
352, and corresponding inspiratory time setting
button 352a may be provided. When the inspiratory
time setting button 352a is depressed, the value
setting of 300 may be utilized to dial in the
15 desired inspiratory time. The set inspiratory
time is the time period for the inspiratory phase of
a pressure control breath. Thus, this inspiratory
time setting is normally usable for pressure control
ventilation.

20 It is preferable that the range of setable
inspiratory times being from 0.3 to 10.0 seconds.

12. Additional Displays/Settings

25 Additional digital displays 344, 346, 354, 356
and corresponding setting buttons 344a, 346a, 354a,
356a are provided to permit the controller 12 to be
subsequently programmed or expanded to receive and
display additional control settings beyond those
which have been described hereabove.

13. Sigh On/Off

30 A sigh on/off button 360 is provided. When
sigh on/off button 360 is depressed, the controller
12 will cause the ventilator 14 to deliver a sigh
breath. A sigh breath is a volume-controlled,
mandatory breath that is usually equal to 1.5 times
35 the current tidal volume setting shown on tidal
volume setting display 332. The sigh breath is
delivered according to the current peak flow setting

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shown on peak flow setting display 336. The inspiratory phase of the sigh breath is preferably limited to a maximum of 5.5 seconds. During a sigh breath, the breath period is automatically increased
5 by a factor of 1.5. The sigh breath function is available during all ventilation modes.

A single depression of the sigh on/off button 348 will cause the ventilator to deliver a volume-controlled sigh breath once every 100 breaths or
10 every 7 minutes, which ever comes first. The sigh breath button 360 includes a visual indicator light 360a which illuminates when the sigh on/off button 360 is depressed and the sigh/breath function is active.

15 **14. Manual Breath**

A manual breath button 362 is also provided. Upon depression of the manual breath button 362, the controller 12 will cause the ventilator 14 to deliver a single volume-controlled or pressure-control breath in accordance with the associated volume and/or pressure control settings. An indicator light 362a will illuminate briefly when manual breath button 362 is depressed.
20

15. **Remote Alarm (Optional)**

25 A remote alarm on/off control button 364 is provided to enable or disable the remote alarm. When the remote alarm on/off control button 364 is depressed, indicator light 364a will illuminate. When the remote alarm on/off button 364 is
30 depressed, the remote alarm will be enabled. When this function is enabled, alarm conditions will transmit via hard wire or radio frequency (wireless) to a remote alarm which may be mounted on the outside of a patients room so as to signal attendants outside of the room, when an alarm
35 condition exists.

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The specific alarm conditions which may be utilized with the remote alarm function, are described in greater detail herebelow.

16. Flow Waveform (Optional-Applies To Volume Breaths Only)

5 The controller 12 includes a square flow wave form activation button 366 and a decelerating taper flow wave form actuation button 368. When the square flow wave form actuation button 366 is depressed, indicator light 366a will illuminate, and the ventilator will deliver inspiratory flow at a constant rate according to the peak flow setting, as input and shown on peak flow display 336. When the decelerating paper wave form actuation button 368 is 10 depressed, indicator light 368a will illuminate, and the ventilator will deliver an inspiratory flow which initially increases to the peak flow setting, as input and shown on peak flow display 336, then such inspiratory flow will decelerate to 50 percent 15 of the peak flow setting at the end of the inspiratory phase.

20 17. Inspiratory Hold (Optional)

An inspiratory hold actuation button 370 is provided, to enable the operator to hold the patient 25 at an elevated pressure following inspiration, so that breath mechanics can be calculated. The length of the delay period is determined by the period of time during which the inspiratory hold button 370 remains depressed, with a maximum limit applied.

30 18. Expiratory Hold (Optional)

The controller 12 also includes an expiratory hold actuation button 372, which enables the ventilator to calculate auto PEEP. During the expiratory hold, the turbine 30 operation is halted 35 and the exhalation valve 18 remains closed. The difference between the end expiratory pressure, as measured at the end of the expiratory hold period,

-25-

minus the airway pressure reading recorded at the beginning of the expiratory hold period, will be displayed on monitor window 384.

5 **19. Maximal Inspiratory Pressure/Negative Inspiration Force (Optional)**

The preferred controller 12 also incorporates a maximal inspiratory pressure test button 374, to enable the operator to initiate a maximal inspiratory pressure (MIP) test maneuver. This maneuver causes the ventilator to stop all flow to or from the patient. The patient inspiratory effort is then monitored and displayed as MIP/NIF in the monitor window 384.

10 **20. 100% O₂ Suction (Optional)**

15 Optionally, the controller 12a includes a 100% O₂ actuation button 376 which, when depressed, will cause indicator light 376a to illuminate and will cause the system 10 to deliver an FiO₂ of 1.00 (i.e., 100% oxygen) to the patient for a period of 20 three (3) minutes regardless of the current FiO₂ setting and/or breath type setting.

25 This 100% O₂ feature enables the operator to selectively deliver 100% oxygen to the patient PT for a three minute period to hyperoxygenate the patient PT prior to disconnection of the patient from the ventilator circuit for purposes of suctioning, or for other clinical reasons.

20 **21. Additional Control Actuation Buttons**

30 An additional control actuation button 378, with indicator light 378a, is provided to enable the controller 12a to be subsequently programmed to perform additional control actuation functions beyond those described hereabove.

MONITORS AND INDICATORS

35 **1. AC Power Status Indicator**

An AC power indicator light 304 is provided in the face panel of the controller 12 to indicate when

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sufficient AC power is available and the standby/off switch (not shown) is in the standby position.

2. Internal Battery Status Indicator(s)

An internal battery status indicator light 308
5 is provided on the panel of the controller 12, and will indicate battery charge level according to predetermined color signals. A separate internal battery charge indicator light 306 may be provided, and will indicate charging status according to
10 predetermined color signals.

3. External Battery Status Indicator(s)

An external battery status indicator light 312 is provided on the panel of the controller 12, and will indicate battery charge level according to predetermined
15 color signals. A separate external battery charge indicator light 310 may be provided, and will indicate charging status according to predetermined color signals.

4. Airway Pressure Monitor

The display panel of the controller 12 includes
20 a real time airway pressure bar graph display 380. A green indicator bar will appear on the airway pressure bar graph display 380 to indicate the real time airway pressure at all times. Red indicators will appear on the airway pressure bar graph to indicate high and low peak pressure alarm setting, as more fully described herebelow under the heading
25 "Alarms". An amber colored indicator will appear on the airway pressure bar graph display 380 to indicate the current PEEP/CPAP setting, Pressure Support setting and/or Pressure Control setting. A patient effort indicator light 382 is located near the airway pressure bar graph display 380, and will illuminate to indicate the occurrence of a patient-initiated breath, including all spontaneous, assist or pressure support breaths.
30
35

5. Digital Monitor Display

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The panel of the controller 12 preferably includes a digital monitor display 384 and an accompanying monitor select button 386. The controller 12 is programmed to display various monitored parameters. Each time the monitor select button 386 is depressed, the monitored parameters displayed on monitor display 384 will change. The individual parameters may include: exhaled tidal volume, i.e., ratio, mean airway pressure, PEEP, peak inspiratory pressure, total breath rate, total minute ventilation.

Additionally, a display power saving feature may be incorporated, whereby the controller 12 will automatically cause the monitor display 384 to become non-illuminated after a predetermined display period when the system 10 is operating solely on internal or external battery power. Each time the monitor select button 386 is depressed, the display 384 will illuminate for a predetermined period of time only, and then will become non-illuminated. This feature will enable the system 10 to conserve power when the system 10 is being operated solely on internal or external battery power.

Additionally, the controller 12 may be programmed to cause the monitor display 384 to display a special or different group of parameters during a specific operator-initiated maneuver. Examples of special parameter groups which may be displayed during a specific maneuver include the following:

- Real-time Pressure (at start of and during all maneuvers)
- Plateau Pressure (Inspiratory Hold)
- Compliance (Inspiratory Hold)
- End Expiratory Pressure (Expiratory Hold)
- Auto PEEP (Expiratory Hold)

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- Maximal Inspiratory Pressure (MIP/NIF)

Alarms And Limits

The preferred controller 12 may be programmed to receive operator input of one or more limiting parameters, and to provide audible and/or visual alarm indications when such limiting parameters have been, or are about to be, exceeded.

The visual alarm indicators may comprise steady and/or flashing lights which appear on the control panel of the preferred controller 12a.

The audible alarm components will preferably comprise electronic buzzers or beepers which will emit sound discernable by the human ear for a preselected period (e.g., 3 seconds). Preferably, the audible portion of any alarm may be volitionally muted or deactuated by the operator.

Additionally it is preferable that the controller 12 be programmed to automatically reset each alarm if the current ventilation conditions do not fall outside of the preset alarm limits.

Examples of specific limiting parameters and alarm limits which may be programmed into the preferred controller 12, are as follows:

25 1. High Peak Pressure

The preferred controller 12 includes, on its face panel, a high pressure digital display 390 and a corresponding high pressure alarm limit setting button 390a. When the high pressure alarm limit setting button 390a is depressed, value setting knob 300 may be utilized to dial in a desired high pressure alarm limit value. Such high pressure alarm limit value will then be displayed on high pressure alarm limit display 390.

35 The currently set high pressure alarm limit, as shown on high pressure alarm limit display 390, will establish the maximum peak inspiratory pressure for all breath types. When the monitored airway

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5

pressure exceeds the currently set high pressure alarm limit, audible and visual alarms will be actuated by the controller 12 and the controller will immediately cause the system 10 to cycle to expiratory mode, thereby allowing the airway pressure to return to the baseline bias flow level and along the exhalation valve 18 to regulate pressure at any currently-set peep level.

10

15

In order to avoid triggering of the high pressure alarm during delivery of a sigh breath, the controller 12 will be programmed to automatically adjust the high pressure alarm limit value by a factor of 1.5X during the delivery of a sigh breath, provided that such does not result in the high pressure limit value exceeding 140 cmH₂O. The controller 12 is preferably programmed not to exceed a high pressure limit setting of 140 cmH₂O, even during delivery of a sigh breath.

20

25

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2. Low Peak Pressure
A low peak airway pressure limit display 392, and corresponding low peak pressure limit setting button 392a, are also provided. When the low peak pressure limit setting button 392a is depressed, value setting knob 300 may be utilized to dial in a desired low peak airway pressure alarm limit value. Such low peak pressure alarm limit value will then be displayed in the low peak pressure display 392.

Audible and/or visual alarms will be activated if the monitored airway pressure fails to exceed the low peak pressure alarm limit setting during the inspiratory phase of a machine-cycled mandatory or assist breath.

The controller 12 is preferably preprogrammed to deactivate the low peak airway pressure alarm during spontaneous, CPAP and pressure support breathing.

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The range of low peak pressure settings will preferably be from 2 to 140 cmH₂O.

3. Low Minute Volume

A low minute volume display 394, and corresponding low minute volume setting button 394a are provided. When low minute volume setting button 394a is depressed, value setting knob 300 may be used to dial in the desired low minute volume alarm setting. The currently-set low minute volume alarm setting will be displayed in digital display 394.

The controller 12 will be programmed to calculate the current exhaled minute volume based on information received from the exhalation valve differential pressure transducer 70, and to trigger audible and/or visual alarms when the exhaled minute volume becomes less than or equal to the currently set low minute volume alarm limit. This alarm is active for all breath types.

The typical range of setable low minute volume alarm limits is from 0 to 99.9 liters/min.

4. Apnea Alarm

The controller 12 may be programmed to trigger auditory and/or visual apnea alarms when the period between initiation of inspiratory phases exceeds 20 seconds. The controller 12 is preferably also programmed to initiate back-up machine ventilation when an apnea alarm condition exists.

The controller 12 is preferably programmed not to permit volitional silencing of the apnea alarm until the apnea condition has been corrected.

5. Spare Alarm Limit Displays And Setting Buttons

Spare alarm limit displays 396, 398, and corresponding spare alarm limit setting buttons 396a and 398a are provided, to permit the controller 12 to be subsequently expanded or programmed to receive operator input of additional limiting parameters,

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and to provide auditory and/or visual alarms when such limiting parameters have been exceeded.

6. Ventilator Inoperative

5 A separate ventilator inoperative light indicator 400 is provided on the face panel of the controller 12. The controller 12 is programmed to cause the ventilator inoperative light to illuminate when predetermined "ventilatory inoperative" conditions exist.

10 **7. AC Power Low/Fail**

The controller 12 is preferably programmed to activate visual and/or auditory alarms when an AC power cord is connected to the system 10 and the voltage received by the system 10 is outside of a specified operating range. The controller 12 is preferably also programmed to automatically switch the system 10 to internal battery power under this condition. The AC power low/fail alarm can be silenced, and will remain silenced, until such time as the internal low battery alarm 208 becomes actuated, indicating that the internal battery has become depleted.

15 **8. External/Internal Battery Low/Fail**

20 The controller 12 may be programmed to actuate a visual and or auditory alarm when an external or internal battery is in use, and the battery voltage is outside of an acceptable operating range.

25 **9. O₂ Inlet Pressure**

30 The controller 12 may be programmed to provide auditory and/or visual alarms when the oxygen pressure delivered to the system 10 is above or below predetermined limits.

35 **10. Over Pressure Relief Limit**

The system 10 includes a mechanical variable pressure relief valve 64, to relieve any over pressurization of the patient circuit.

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The range of setable over pressure relief limit values may be between 0 to 140 cmH₂O.

SELF TESTING AND AUTO CALIBRATION FUNCTIONS

1. Self Test Function

5 The preferred controller 12 may be programmed to perform a self-testing function each time the ventilator is powered up. Such self testing function will preferably verify proper functioning of internal components such as microprocessors, memory, transducers and pneumatic control circuits.

10 Such self testing function will also preferably verify that electronic sub-systems are functioning correctly, and are capable of detecting error conditions relating to microprocessor electronics.

15 Also, during power up, the controller 12 may be programmed to allow a qualified operator who enters a given key sequence, to access trouble shooting and calibration information. In accordance with this feature, the key operator may induce the controller to display, on the monitor display 384, information such as the following:

SOFTWARE REVISION

PEAK FLOW AND PRESSURE TRANSDUCER OUTPUT

LAMP TEST/ALL DISPLAYS ON

25 ANY AUTO ZERO AND PURGE FUNCTIONS
FOR THE FLOW PRESSURE TRANSDUCER

EVENT DETECTION MENU INCLUDING PREVIOUS
STATUS OR FAULT CODES

30 REMOTE ALARM TEST AND PROGRAM; and
DATA COMMUNICATIONS TEST AND PROGRAM

Also, the controller 12 may be programmed to allow a qualified operator who entered a given key sequence, to access a user preference and set up menu. Such menu may 35 include a monitory display 384, of information such as the following:

- System lock, enable or disable;
- Variable Apnea interval;
- Language selection; and

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- User verification tests.

The user preference and set up menu function may also be accessible during operation of the system 10.

C. A Preferred Rotary Drag Compressor Apparatus

5 The portable system 10 ventilator of the present invention preferably incorporates a rotary drag compressor apparatus 30 comprising a dual-sided, multi-bladed rotor 104 disposed within a rigid compressor housing 106. An inflow/outflow manifold 108 is formed integrally with the compressor housing 106, and incorporates two (2) inflow passageways 112 and two (2) outflow passageways 110 for channeling gas flow into and out of the compressor apparatus 30.

An electric motor 102, such as a 0.8 peak horsepower, 40 volt D.C. motor, is preferably mounted integrally within the compressor housing 106. Alternatively, the motor 102 may be encased or housed in an encasement or housing which is separate from the compressor housing 106. The motor shaft 114 extends transversely into a bore 116 formed in the central hub 118 of rotor 104. As shown, the bore 116 of the central hub 118 of rotor 104 may include a rectangular key-way 121 formed on one side thereof and the motor shaft 114 may include a corresponding elongate rectangular lug formed thereon. The rectangular lug of the motor shaft 114 inserts within and frictionally engages the key-way 121 of the rotor hub 118, thereby preventing the motor shaft 114 from rotationally slipping or turning within the bore 116 of the rotor hub 118. It will be appreciated however, that various alternative mounting structures, other than the lug and keyway 121 shown in Figures 8-9, may be utilized to rotatably mount the motor shaft 114 to the rotor 104.

35 The rotor hub 118 is preferably formed having a concave configuration, as shown in Figure 5. Such concave configuration serves to impart structural integrity and strength to the rotor 104, without

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significantly increasing the mass of the rotor 104 as would result from the formation of additional strengthening ribs or bosses on the rotor hub 118.

As shown in Figures 5-10, a first annular trough 120 5 extends about the periphery of the front side of the rotor 104, and a second annular trough 122 extends about the periphery of the backside of the rotor 104.

A multiplicity of rotor blade-receiving slots 126 are formed angularly, at evenly spaced intervals about 10 the inner surfaces of the first 120 and second 122 annular troughs. Rotor blades 128 are mounted at spaced-apart locations around each annular trough 120, 122 such 15 that the radial peripheral edge 127 of each blade 128 is inserted into and resides within a corresponding blade receiving slot 126 and the leading edge 129 of each blade traverses across the open annular trough 120 or 122, as shown. Each blade 128 is affixed by adhesive, or other suitable means, to the body of the rotor 104.

In the preferred embodiment the blades 128 are 20 located in axially aligned positions, i.e., non-staggered directly opposite positions on opposite sides of the rotor 104 so as to promote even pressure balance and symmetrical weight distribution within the rotor 104.

The rotor 104 is rotatably mounted within the 25 compressor housing 106 such that the first 120 and second 122 annular cavities are in alignment with the inflow 110 and outflow 112 channels, as shown.

In order to optimize the controllability of the 30 rotor 104 velocity, and to minimize the wear or stress on the system drive components from repeated abrupt starting and stopping of the rotor 104, it is desirable that the overall mass of the rotor 104 be minimized. Toward this end, the body of the rotor 104 is preferably constructed of light weight material such as aluminum, and the 35 individual blades 128 of the rotor 104 are preferably constructed of light weight material such as glass-filled epoxy. In embodiments where the body of the rotor 104 is

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formed of aluminum and the blades 128 are formed of glass-filled epoxy, a suitable adhesive such as epoxy may be utilized to bond the radial edges of the blades 128 within their corresponding blade-receiving slots 126.

5 Alternatively, it is contemplated to form the rotor and blades integrally, as by way of a molding process whereby metal (e.g., aluminum), polymer or composite materials are molded to form the blades 128 and rotor 104 as a unitary structure.

10 After the rotor blades 128 have been mounted and secured in their respective blade-receiving slots 126, each individual blade 128 will preferably be disposed at an angle of attack A, relative to a flat transverse plane TP projected transversely through the body of the rotor 104, between the first annular trough 120 on the front side of the rotor 104, and the second annular trough 122 on the backside of the rotor 104. The angle A is preferably in the range of 30-60 degrees and, in the preferred embodiment shown in Figures 8-10 is 55 degrees.

15 Such angle A is selected to provide optimal flow-generating efficiency of the rotor 104.

20 In operation, it is necessary to precisely control the timing of the acceleration, deceleration, and the rotational speed, of the rotor 104 in order to generate a prescribed inspiratory pressure and/or flow rate and/or volume. Although standard manufacturing tolerances may be maintained when manufacturing the rotor 104 and other components of the compressor 30 (e.g., the rotor 104, compressor housing 106, motor 102) each individual compressor 30 will typically exhibit some individual variation of flow output as a function of the rotational speed and differential pressure of that compressor 30. Thus, in order to optimize the precision with which the inspiratory flow may be controlled, it is desirable to obtain precise flow and pressure data at various turbine speeds for each individual compressor 30, and to provide such characterization data to the controller 12 to enable

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the controller 12 to adjust for individual variations in the pressure and/or flow created by the particular compressor 30 in use. As a practical matter, this may be accomplished in either of two ways. One way is to 5 generate discrete flow rate, speed and pressure measurements for each compressor 30 at the time of manufacture, and to provide a table of such discreet flow rate, speed and pressure values to the ventilator controller 12 at the time the particular compressor 30 is 10 installed. The controller 12 will be correspondingly programmed to perform the necessary interpolative mathematical steps to obtain instantaneous flow, speed or pressure determinations as a function of any two such variables, for the particular compressor 30. The second 15 way is to experimentally generate a series of flow, speed and pressure data points over a range of normal operating rotor speeds, and to subsequently derive a unique speed vs. flow vs. pressure equation to characterize each individual compressor 30. Such individual 20 characterization equation is then programmed into, or otherwise provided to, the controller 12 and the controller 12 is programmed to utilize such equation to compute precise, instantaneous speed, flow rate and pressure control signals for controlling the individual 25 compressor 30 in use. An example of such graphical speed vs. flow rate vs. pressure data, and a characterization equation derived therefrom, is shown in Figure 12.

Given the current cost of microprocessor technology, providing a controller 12 which has the capability to 30 receive and process such a characterization equation as shown in (Figure 12) for controlling the compressor 30 would require substantial expense and size enlargement of the controller 12. Accordingly, given the present state of the art, it is most desirable to utilize the former of 35 the two above-described methods -- that is, providing a database of discrete flow, speed and pressure values and programming of the controller 12 to perform the necessary

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mathematical interpolations of the provided data points for maintaining compressor-specific control of the pressure, flow rate and/or volume of gas provided in each inspiratory phase at the ventilation cycle. The 5 experimentally generated database of discreet flow, speed and pressure valves may be encoded onto an EPROM or any other suitable database storage device. Such EPROM or other database storage device may be located on or within the compressor 30 itself and communicated to the 10 controller 12 via appropriate circuitry. Alternatively, such EPROM or database storage device may be installed directly into the controller 12 at the time the particular compressor 30 is installed within the ventilator device 14.

15 The controlled inspiratory flow generated by the rotary drag compressor 30, exists from the compressor outlet 34 and through line 22 to the patient PT. As shown in Figure 2, an output silencer 60, such as a hollow chamber having a quantity of muffling material 20 formed therearound, is preferably positioned on inspiratory flow line 22 to reduce the sound generated by the ventilator 14 during operation. An inspiration occlusion valve 62 is additionally preferably mounted on inspiratory flow line 22 to accomplish operator 25 controlled stoppage of the inspiratory flow as required during performance of a maximal inspiratory force maneuver. Additionally, a pressure relief valve 64 is connected to inspiratory flow line 22 to provide a safeguard against delivering excessive inspiratory 30 pressure to the patient PT. The pressure relief valve 64 may be manually set to the desired limit pressure, by the operator.

In general, the rotary drag compressor ventilator 14 operates by periodic rotating of the rotor 130 within the 35 compressor 30 to generate the desired inspiratory gas flow through line 22. It is desirable that the rotor 130 be accelerated and decelerated as rapidly as possible.

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Such rapid acceleration/deceleration is facilitated by a reduction in inertial effects as a result of the above-described low mass construction of the rotor 104. The speed and time of rotation of the rotor 104, during each 5 inspiratory phase of the ventilator cycle, is controlled by the controller 12 based on the variables and/or parameters which have been selected for triggering, limiting and terminating the inspiratory phase.

The precise flow, volume or pressure delivered 10 through the inspiratory line 22 is controlled by the controller based on the EPROM-stored compressor characterization data received by the controller, as well as periodic or continuous monitoring of the rotational speed of the rotor 104 and the change in pressure (Δ_p) 15 between the inlet side 32 and outlet side 34 of the compressor 30 as monitored by the differential pressure transducer 36.

In the presently preferred embodiment, the controller 12 is programmed to deliver breaths by either 20 of two available closed loop algorithms; volume or pressure.

Example: Volume Breaths

Prior to Volume breath initiation, the controller 12 generates a predefined command waveform of flow vs time. The waveform is generated using the current Flow, Volume and Waveform input settings from the front panel. Since the mathematical integral of flow over time is equal to the volume delivered, the 25 controller can determine the appropriate inspiratory time.

Once a volume breath has been triggered, the controller uses closed loop control techniques well known in the art to drive the compressor, periodically read the compressor differential pressure and rotational speed, and then calls 30 upon the specific stored compressor

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characterization data to arrive at the actual flow rate. Once actual flow rate is known, it is compared or "fed back" to the current commanded flow, and a resulting error is derived. The error is then processed through a control algorithm, and the compressor speed is adjusted accordingly to deliver the desired flow rate. This process is repeated continuously until the inspiration is complete.

Example: Pressure Breaths

Pressure breaths include several breath types such as Pressure Support or Pressure Control. In these breath types, the controller commands the compressor to provide flow as required to achieve a pressure as input from the front panel.

Once a pressure breath has been triggered, the controller uses closed loop control techniques well known in the art to drive the compressor 30 and to achieve the desired patient airway pressure. The controller periodically reads the actual airway pressure. Once actual pressure is known, it is "fed back" and compared to the current commanded pressure, and a resulting error is derived. The error is then processed through a control algorithm, and the compressor speed is adjusted accordingly to deliver the desired pressure. This process is repeated continuously until the inspiration is complete.

For both breath types, once the selected inspiratory termination variable is reached, the controller will signal the compressor motor 102 to stop or decelerate to a baseline level, thereby cycling the ventilator in to the expiratory phase.

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D. A Preferred Oxygen Blending Apparatus

When oxygen enrichment of the inspiratory flow is desired, the controller 12 may be additionally programmed or equipped to control the operation of the oxygen blending apparatus 16 to mix a prescribed amount of oxygen with ambient air drawn through air intake 24, thereby providing an inspiratory flow having a prescribed oxygen content (FiO_2) between 21% - 100%.

5 blending apparatus 16 to mix a prescribed amount of oxygen with ambient air drawn through air intake 24, thereby providing an inspiratory flow having a prescribed oxygen content (FiO_2) between 21% - 100%.

As shown in Figures 2 and 3, the preferred oxygen blending apparatus 16 comprises an air inlet line 24 which opens into a hollow vessel or accumulator 54.

10 blending apparatus 16 comprises an air inlet line 24 which opens into a hollow vessel or accumulator 54.

Oxygen inlet line 26 is connected to a pressurized source of oxygen and leads, via a manifold to a series of solenoid valves 52. Although not by way of limitation, 15 in the preferred embodiment as shown in Figure 3, five (5) separate solenoid valves 52a-52e are utilized. Each such separate solenoid valve 52a-52e has a specific (usually differing) sized flow restricting orifice formed therein so that each such solenoid valve 52a-52e will 20 permit differing amounts of oxygen to pass into accumulator 54, per unit of time during which each such solenoid valve 52a-52e is maintained in an open position. The controller 12 is preprogrammed to determine the specific period(s) of time each solenoid valve 52a-52e 25 must remain open to provide the necessary amount of oxygen to accumulator 54 to result in the prescribed oxygen concentration (FiO_2).

Algorithm for a Preferred Oxygen Blending Apparatus

The rotational velocity of the rotor 104 and 30 differential pressure across the inflow/outflow manifold 108 are measured by the controller 12 and from this data the controller 12 is able to determine the flow of gas through the compressor 30 from the accumulator 54. The controller 12 integrates the air flow drawn through the 35 compressor 30 to determine the accumulated volume of enriched gas drawn from said accumulator 54. In order to maintain the flow of gas at the prescribed FiO_2 level, a

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portion of this removed volume must be replaced in the accumulator 54 with pure oxygen.

The accumulated volume is compared to a predetermined trigger volume for each of the solenoids 5 52a-52e, which in the preferred embodiment, is defined by the equation:

$$\text{Trigger Volume} = (\text{Solenoid Flow} * \text{Time} * 79) / [(\text{FiO}_2 - 21) * 2]$$

Starting with the smallest, each solenoid that is 10 not currently open is compared. When the accumulated volume reaches the trigger volume for a solenoid 52, the controller 12 opens that solenoid 52 for a period of time allowing oxygen to flow from the oxygen inlet line 26 through the solenoid 52 and into the accumulator 54. The 15 controller 12 then adjusts the accumulated volume appropriately by subtracting a volume, proportional to the volume of oxygen delivered to the accumulator 54 from the accumulated volume defined by the equation:

$$\text{Subtracted Volume} = (\text{Solenoid Flow} * \text{Time} * 79) / (\text{FiO}_2 - 20 21).$$

This process is repeated continuously.

The trigger volume the controller 12 uses to open an individual solenoid 52a-52e is independent for each 25 solenoid 52 and is function of the flow capacity of the particular solenoid 52a-52e, the prescribed FiO_2 level, and the amount of time the solenoid 52 is open. In the preferred embodiment, the amount of time each solenoid 52 is open is the same for each solenoid 52, but may vary as a function of oxygen inlet pressure.

30 **Example: Delivery of 0.6 FiO_2 Using 4 Solenoids**

In this example, the oxygen blending apparatus has 4 solenoids with flows of 5 lpm, 15 lpm, 40 lpm, and 80 lpm respectively. The FiO_2 setting is 60%, thus the trigger volumes for each of the 4 solenoids is 8 ml, 25 35 ml, 66 ml, and 133 ml respectively. Furthermore a constant oxygen inlet pressure is assumed resulting in an "on" time of 100 ms for the solenoids, a constant

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compressor flow of 60 lpm, and a period of 1 ms. The following table describes the state of the oxygen blending algorithm after various iterations:

	Time (ms)	Accumulated Volume (ml)	Solenoid 1 (8 ml)	Solenoid 2 (25 ml)	Solenoid 3 (66 ml)	Solenoid 4 (133 ml)
5	0	0	off	off	off	off
	1	1	off	off	off	off
	2	2	off	off	off	off
	**					
10	7	7	off	off	off	off
	8	0	on	off	off	off
	9	1	on	off	off	off
	**					
15	32	24	off	off	off	off
	33	0	on	on	off	off
	34	1	on	on	off	off
	**					
20	98	65	on	on	off	off
	99	0	on	on	on	off
	100	1	on	on	on	off
	**					
25	107	8	on	on	on	off
	108	1	off>on*	on	on	off

*At 108 ms the 8 ml solenoid turned off after having been on for 100ms, but since the accumulated volume is now 9 ml the solenoid is turned on again.

Thus, by independently operating the four (4) separate solenoids as shown in the above table, a 0.6 F_O₂ is consistently delivered through the compressor 30.

30 E. A Preferred Exhalation Valve and Exhalation Flow Transducer

Referring generally to Figures 11a-11e the preferred exhalation valve and exhalation flow transducer assembly of the present invention is depicted. By way of overview, the exhalation valve 18 comprises a housing

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which defines an expiratory flow path therethrough and a valving system for controlling the airway pressure during the expiratory phase of the ventilation cycle. The exhalation valve 18 shares numerous structural and 5 functional attributes with the exhalation valve described in United States Number 5,127,400 (DeVries et al) entitled Ventilator Exhalation Valve, issued July 7, 1994, the disclosure of which is expressly incorporated herein by reference.

10 In addition, the exhalation valve assembly 18 of the present invention additionally incorporates an exhalation flow transducer 230 which serves to monitor exhalation flow from the patient and generates an output signal to the controller 12. The output signal is then utilized by 15 the controller to determine when patient exhalation has ceased to thereby initiate inspiratory flow to the patient. In the preferred embodiment, the exhalation flow transducer 230 is mounted within the exhalation valve 18 in unique structure to minimize manufacturing 20 inaccuracies. Further, in the preferred embodiment, the particular operational characteristics of the exhalation flow transducer 230 are stored within a memory device which is then communicated to the controller 12 to insure accuracy in flow measurements. The exhalation flow 25 transducer 230 of the present invention shares numerous structural and functional attributes with the flow transducer described in the United States Patent Number 4,993,269, issued to Guillaume et al., entitled Variable Orifice Flow Sensing Apparatus, issued on February 19, 30 1991, the disclosure of which is expressly incorporated herein by reference.

Referring more particularly to Figures 11a through 11e, the exhalation valve 18 of the present invention is formed having a housing 200 including an exhalation 35 tubing connector 202 formed at a first location thereon and an outflow port 204 formed at a second location thereon. An exhalation gas flow passageway 206 extends

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through the interior of the housing 200 such that expiratory gas may flow from the exhalation tubing connector 202 through the exhalation passageway 206 within the interior of the exhalation valve 18 and subsequently passed out of the outflow port 204. Midway through the expiratory flow passageway 206, there is formed an annular valve seat 208. The annular valve seat 208 may be disposed in a plane which is parallel to the plane of the flat diaphragm 210 or alternatively, as in the embodiment shown, the annular valve seat 208 may be slightly angled or tapered relative to the plane in which the flat diaphragm 210 is positioned. Such angling or tapering of the valve seat 208 facilitates seating of the diaphragm 210 on the valve seat 208 without flutter or bouncing of the diaphragm 210. The elastomeric disc or diaphragm 210 is configured and constructed to initially contact the farthest extending side of the angled valve seat 208, and to subsequently settle or conform onto the remainder of the angled valve seat 208, thereby avoiding the potential for flutter or bouncing which may occur when the diaphragm 210 seats against a flat non-angled valve seat 208.

The disc or diaphragm 210 is preferably attached to the surrounding rigid housing 200 by way of an annular flexible frenulum 212. Frenulum 212 serves to hold the disc or diaphragm 210 in axial alignment with the annular valve seat 208, while permitting the disc or diaphragm 210 to alternatively move back and forth between a closed position wherein the diaphragm 210 is firmly seated against the valve seat 208 (Figure 11a) and a fully open position wherein the disc or diaphragm 210 is retracted rearwardly into the adjacent cavity within the housing 200 thereby providing an unrestricted flow path 206 through which expiratory gas may flow.

A pressure distributing plate 214 is mounted on the backside of the diaphragm 210. A hollow actuation shaft 216 is mounted within the housing 200 and is axially

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reciprocal back and forth to control the position of the diaphragm 210 relative the valve seat 208. A bulbous tip member 218 is mounted on the distal end of a hollow actuation shaft 216. A corresponding pressure distribution plate 214 is mounted on the back of the diaphragm 210. Forward movement of the actuation shaft 216 causes the bulbous tip member 218 to exert forward pressure against the plate 214 thereby forcing the diaphragm 210 toward its closed position. When the actuation shaft 216 is in a fully forward position, the diaphragm 210 will be held in firm abutment against the annular valve seat 208 thereby terminating flow through the passage 206. Conversely when the actuation shaft 216 is retracted, the diaphragm 210 moves away from the valve seat 208 thereby allowing flow through the passageway 206 thereby allowing flow through the passageway 206.

The movement of the shaft 216 is controlled by way of an electrical induction coil 220 and spider bobbin 222 arrangement. In the preferred embodiment, the electrical induction coil 220 is formed without having an internal support structure typically utilized in induction coils so as to minimize inertial concerns. In this regard, the coil 220 is typically formed by winding upon a mandrel and subsequently maintained in this wound configuration by way of application of a suitable binder or varnish. Additionally, in the preferred embodiment, the bobbin 222 is preferably formed having a cross-beam construction, as shown in Figure 11b, to decrease the mass of the bobbin 222 while maintaining its structural integrity. Similarly, the shaft 216 is preferably formed from a hollow stainless steel material so as to be relatively strong yet light weight enough for minimizing inertial concerns.

As shown, the bobbin 222 is affixed to the distal end of the induction coil 220 and the shaft 216 extends through an aperture formed in the center of the bobbin and is frictionally or otherwise affixed to the bobbin

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such that the shaft 216 will move back and forth in accordance with the bobbin 222 and coil 220. As the current passing into the induction coil 220 increases, the coil 220 will translate rearwardly into the coil receiving space 226 about the magnet thereby moving the shaft 216 and blunt tip member 218 in the rearward direction and allowing the diaphragm 210 to move in an open position away from the valve seat 208 of the expiratory flow path 206. With the diaphragm 210 in such open position, expiratory flow from the patient PT may pass through the expiratory flow pathway 206 and out the expiratory port 204.

Conversely, when the expiratory flow has decreased or terminated, the current into the induction coil may change direction, thereby causing the induction coil to translate forwardly. Such forward translation of the induction coil 220 will drive the bobbin 222, shaft 216, and bulbous tip member 218 in a forward direction, such that the bulbous tip member 218 will press against the flow distributing plate 214 on the backside of the diaphragm 210 causing the diaphragm to seat against the valve seat 208. With the diaphragm 210 seated against the valve seat 208, the inspiratory phase of the ventilator cycle may begin and ambient air will be prevented from aspirating or backflowing into the patient circuit through the exhalation port 204.

In the preferred embodiment, a elastomeric boot 217 or dust barrier is mounted about the distal portion of the hollow actuation shaft 216, and is configured and constructed to permit the shaft 216 to freely move back and forth between its fully extended closed position and a fully retracted open position while preventing dust or moisture from seeping or passing into the induction coil 220.

As best shown in Figure 11, Figures 11a and 11c, the housing of the exhalation valve 18 includes a frontal portion formed by the housing segments 200b, 200c, and

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200d. An airway pressure passage 241 is provided within the housing portion 200b, which enables the pressure within the exhalation passageway 206 to be communicated to an airway pressure tubing connector 233. Airway 5 pressure tubing connector 233 is connected via tubing to an airway pressure transducer 68 (shown in Figure 2) which monitors airway pressure and outputs a signal to the controller 12. Based upon desired operating conditions, the controller 12, in response of receipt of 10 the pressure signal from pressure transducer 68 increases or decreases the voltage applied to the coil 220 to maintain desired pressure within the exhalation air passage 206. As will be recognized, such monitoring of the airway pressure is continuous during operation of the 15 ventilator cycle.

As previously mentioned, the exhalation flow transducer 230 of the present invention is preferably disposed with the exhalation valve housing and serves to monitor exhalation flow from the patient PT. More 20 particular, the exhalation flow transducer 230 of the present invention preferably incorporates a feedback control system for providing real time monitoring of the patient's actual expiratory flow rate. As best shown in Figure 11a and 11c, the expiratory flow transducer 230 of 25 the present invention is incorporated within the exhalation flow path 206 within housing segment 200b. The flow transducer 230 is preferably formed from a flat sheet of flexible material having a cut out region 406 formed therein. A peripheral portion 408 of the flat sheet exists outside of the cut out region 406 and flapper portion 231 is defined within the cut out region 406. Frame members 410 and 412 preferably formed of a polymer material, are mounted on opposite sides of the flat sheet so as to exert inward clamping pressure on the 30 peripheral portion 408 of the flat sheet. The flapper portion 231 of the flat sheet is thus held in its desired 35 transverse position within the open central aperture 14a

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and 14b of the transducer assembly, and such flapper portion 231 is thus capable of flexing downstream in response to exhalation flow.

To minimize the inducement of stresses within the
5 flow transducer assembly 230, a frame member 411 is
preferably positioned in abutting juxtaposition to the
outboard surface of at least one of the frame members
410, 412. In the preferred embodiment shown in Figure
11c, the frame member 411 is positioned in abutment with
10 the upper frame member 410. Such frame member 411
comprises a metal frame portion 413 and includes an
elastomeric cushioning gasket or washer 415 disposed on
the lower side thereof. A central aperture 14c is formed
in the frame member 411, such aperture 14c being of the
15 same configuration, and in axial alignment with central
apertures 14a, 14b of the upper and lower frame members
410, 412.

Upper and lower abutment shoulders 418a, 418b, are
formed within the exhalation valve housing 200 to
20 frictionally engage and hold the flow transducer assembly
230 in its desired operative position. When so inserted,
the upper engagement shoulder 418a will abut against the
upper surface of the frame member 411, and the lower
abutment shoulder 418b will abut against the lower
25 surface of the lower frame member 412, thereby exerting
the desired inward compressive force on the flow
transducer assembly 230. As will be recognized, the
inclusion of the cushioning washer 415 serves to evenly
distribute clamping pressure about the peripheral portion
30 408, thereby minimizing the creation of localized stress
within the flow transducer 230.

When the transducer assembly 230 is operatively
positioned between the upper and lower abutment shoulders
418a, 418b, an upstream pressure port 232 will be located
35 upstream of the flapper 231, and a downstream pressure
port 234 will be located downstream of the flapper 231.
By such arrangement, pressures may be concurrently

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measured through upstream pressure port 232 and downstream pressure port 234 to determine the difference in pressures upstream and downstream of the flapper 231.

As expiratory gas flow passes outwardly, through the 5 outlet port of the exhalation valve 18, the flapper portion 231 of the flow transducer 230 will deflect or move allowing such expiratory gas flow to pass thereacross, but also creating a moderate flow restriction. The flow restriction created by the flow 10 transducer 230 results in a pressure differential being developed across the flow transducer 230. Such pressure differential may be monitored by pressure ports 232 and 234 disposed on opposite side of the flow transducer 230 (as shown in Figure 11a) which pressure ports are in flow 15 communication by internal passages formed within the housing segment 200c, 200b and 200a to tubing connections 240 and 235. A manifold insert 201 may be mounted on the upstream pressure port 232 such that the manifold insert 201 protrudes into the expiratory flowpath 206, upstream 20 of the flapper 231. A plurality of inlet apertures 201a, preferably four in number are formed around the outer sidewall of the manifold insert 201, and communicate through a common central passageway with the upstream pressure port 232, thereby facilitating accurate 25 measurement of the pressure within the expiratory flowpath 206 at that location.

An exhalation differential pressure transducer 70 (shown in Figure 2) may be located within the housing or enclosure of the ventilator 10. The exhalation 30 differential pressure transducer 70 is connected by way of tubing to the first and third pressure port tubing connectors 240 and 235 so as to continuously measure and provide the controller 12 with the difference between pressure upstream (P1) and pressure downstream (P2) of 35 the flow transducer 230. The difference in pressure determined by the exhalation differential pressure transducer 70 is communicated to the controller, and the

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controller is operatively programmed to calculate the actual flow rate at which expiratory gas is exiting the flow channel 206. As will be recognized, the exhalation flow rate may be utilized by the controller 12 for differing purposes such as triggering of initiation of the next inspiratory cycle. Although the particular formation and mounting structure utilized for the exhalation flow transducer 230 provides exceptional accuracy in most situations, the applicant has found that in certain circumstances, it is desirable to eliminate any inaccuracies caused by manufacturing and assembly tolerances. As such, in the preferred embodiment, the specific operational characteristics of each exhalation flow transducer 230, i.e., pressure differential for specific flow rates are measured for calibration purposes and stored on a storage medium contained within the exhalation valve housing 18. In the preferred embodiment this specific characterization and calibration information is encoded on a radio frequency transponder 203 of the type commercially available under the product name Tiris, manufactured by Texas Instruments, of Austin, Texas. The radio-frequency transponder 203 and its associated transmitter/receiver antenna 203a may be mounted within the exhalation valve housing 200 as shown in Figure 11c. Additionally, a radio frequency transmitter/receiver is positioned within the ventilator system 10, such that upon command of the controller 12, the calibration and characterization data contained within the transponder 203 is transmitted via radio frequency to the receiver and stored within the controller 12. Subsequently, the controller 12 utilizes such stored calibration and characterization data to specifically determine expiratory flow rate based upon pressure differential values generated by the differential pressure transducer 70.

F. A Preferred Auto Calibration Circuit

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In the preferred embodiment, the ventilator device 14 of the ventilator system 10 of the present invention incorporates an auto calibration circuit for periodic rezeroing of the system to avoid errors in the tidal 5 volume or inspiratory flow delivered by the drag compressor 30.

In particular, as shown in Figure 2 the preferred auto calibration circuit comprises the following components:

- 10 a) a first auto-zero valve 74 on the line between the inlet 32 of the compressor 30 and the differential pressure transducer 36;
- 15 b) a second auto-zero valve 76 on the line between the first pressure port of the exhalation valve 18 and the first pressure (P1) side of the exhalation differential pressure transducer 70;
- 20 c) a third auto-zero valve 80 on the line between the second pressure (P2) port 234 of the exhalation valve 18 and the second pressure (P2) side of the exhalation differential pressure transducer 70;
- 25 d) a fourth auto-zero valve 78 on the line between the outlet port 34 and the differential pressure transducer 36; and
- e) and a fifth auto-zero valve 72 on the line between the airway pressure port 241 and the airway pressure transducer 68.

Each of the auto-zero valves 72, 74, 76, 78, 80 is connected to the controller 12 such that, at selected 30 time intervals during the ventilatory cycle, the controller 12 may signal the auto-zero valves 72, 74, 76, 78, 80 to open to atmospheric pressure. While the auto-zero valve 72, 74, 76, 78, 80 are open to atmospheric pressure, the controller 12 may re-zero each of the 35 transducers 36, 68, 70 to which the respective auto-zero valve 72, 74, 76, 80 are connected. Such periodic re-zeroing of the pressure transducers 36, 68 and 70 will

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correct any baseline (zero) drift which has occurred during operation.

Ventilator Operation

With the structure defined, the basic operation of 5 the ventilator system 10 of the present invention may be described. As will be recognized, the particular ventilatory mode selected by a technician may be input to the controller 12 via the input controls upon the display 380. Additionally, the technician must attach the 10 inspiratory and exhalation tubing circuit to the patient PT as illustrated in Figure 1.

Prior to initiation of patient ventilation, the controller 12 initiates its auto calibration circuit and system check to insure that all system parameters are 15 within operational specifications. Subsequently, inspiration is initiated wherein the controller 12 rapidly accelerates the drag compressor 30. During such acceleration, air is drawn through the filter 50, accumulator 54 and supplied to the patient PT, via line 20 22. During such inspiratory phase, the controller 12 monitors the pressure drop across the compressor 30, via pressure transducer 36, and the rotational speed of the rotor 104. This data is then converted to flow by the controller 12 via the turbine characterization table to 25 insure that the proper flow and volume of inspiratory gas is delivered to the patient PT. Additionally, during such inspiratory phase, the exhalation valve 18 is maintained in a closed position. In those applications where oxygen blending is desired, the controller 12 30 additionally opens selected ones of the solenoid valve 52a, 52b, 52c, 52d and 52e, in timed sequence to deliver a desired volume of oxygen to the accumulator 54, which is subsequently delivered to the patient PT during inspiratory flow conditions.

35 When inspiratory flow is desired to be terminated, the controller 12 rapidly stops or decelerates the drag compressor 30 to a basal rotational speed, and the

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patient is free to exhale through exhalation line 66 and through the exhalation valve 18. Depending upon desired ventilation mode operation, the controller 12 monitors the exhalation pressure, via pressure transducer 68 connected to the airway passage and adjusts the position of the valve relative the valve seat within the exhalation valve 18 to maintain desired airway pressures. Simultaneously, the controller 12 monitors the pressure differential existing across the exhalation flow transducer 230 via exhalation pressure transducer 70 to compute exhaled flow. This exhaled flow is used to compute exhaled volume and to determine a patient trigger. When a breath is called for either through a machine or patient trigger, the controller initiates a subsequent inspiratory flow cycle with subsequent operation of the ventilator system 10 being repeated between inspiratory and exhalation cycles.

Those skilled in the art will recognize that differing ventilation modes, such as intermittent mandatory ventilation (IMV), synchronized intermittent mandatory ventilation (SIMV) controlled mechanical ventilation (CMV) and assist control ventilation (A/C), are all available modes of operation on the ventilator 10 of the present invention. Further those skilled in the art will recognize that by proper selection of control inputs to the ventilator 10, all modern breath types utilized in clinical practice, may be selected, such as machine cycled mandatory breath, machine cycled assist breath, patient cycled supported breath, patient cycled spontaneous breath, volume controlled mandatory breaths, volume controlled assist breaths, pressure controlled breaths, pressure support breaths, sigh breaths, proportional assist ventilation and volume assured pressure support.

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WHAT IS CLAIMED IS:

1. A rotary drag compressor ventilator device for ventilating the lungs of a mammalian patient, said device comprising:

5 A. a rotary drag compressor comprising:
 i. a housing having a gas inflow passageway and a gas outflow passageway;

10 ii. a rotor mounted within said housing, said rotor having a multiplicity of blades formed circularly therearound such that, when said rotor is rotated in a first direction, said blades will compress gas within said housing and expel said compressed gas out of said outflow passageway;

15 iii. a motor coupled to said compressor for rotating said rotor within said compressor housing; and

20 B. a controller apparatus to intermittently accelerate and decelerate the rotation of said rotor so as to deliver discrete periods of inspiratory gas flow through said outflow passageway.

25 2. The ventilator of Claim 1, further in combination with:

25 C. an oxygen blending apparatus connected to said inflow passageway for blending oxygen with ambient air to provide oxygen-enriched air to the inlet aperture of said compressor housing.

30 3. The ventilator of Claim 2 wherein said oxygen blending apparatus comprises:

30 an ambient air receiving passageway;
 an oxygen receiving passageway;
 an accumulator for receiving ambient air through said ambient air passageway and oxygen through said oxygen passageway; and,

35 a series of independently actuatable solenoid valves positioned, in parallel, within the oxygen receiving passageway of said bending apparatus, each

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of said solenoid valves having a predetermined flow rate when fully open, each of said solenoid valves thereby permitting passage therethrough of a predetermined amount of oxygen per time period; and,

5 said oxygen blending apparatus being connected to said controller and said controller being further programmable to receive input of a desired oxygen concentration setting and to emit control signals to the solenoid valves to cause individual opening and
10 closing of said solenoid valves to result in said desired oxygen concentration within said accumulator.

4. The ventilator system of Claim 3 wherein said solenoid valves comprises three to five separate solenoid
15 valves.

5. The ventilator system of Claim 3 wherein said controller is programmed to apply a pulse-width modulation signal to control the opening and closing of said solenoid valves.

20 6. The ventilator of Claim 1 wherein said controller comprises at least one microprocessor.

7. The ventilator of Claim 1 wherein said compressor rotor comprises a dual-faced compressor rotor having first and second series of blades mounted opposite
25 sides thereof; and, wherein said compressor housing is configured to define first and second compressor flow paths which are positioned in relation to said first and second series of blades, respectively, such that rotation of said compressor rotor in said first direction will a)
30 draw gas into said inflow passageway, b) concomitantly compress and move gas through both of said first and second flow paths and, c) expel the combined gas from said first and second compressor flow paths to compressor flow paths to provide inspiratory gas flow from said
35 ventilator device.

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8. The ventilator of Claim 7 wherein said compressor rotor is round in configuration and has a diameter of 2-6 inches.

5 9. The ventilator of Claim 7 wherein said blades are disposed at angles of attack of 30-60 degrees.

10 10. The ventilator of Claim 9 wherein said blades are disposed at 55° angles of attack.

11. The compressor of Claim 7 wherein said blades are mounted within concave annular troughs formed on opposite sides of said dual-faced compressor rotor and wherein said first and second compressor flow paths are formed in relation to said first and second annular troughs such that the series of blades mounted within the first annular trough will compress gas within said first 15 compressor flow path and the series of blades mounted within said second trough will compress gas within said second compressor flow path.

12. The ventilator of Claim 7 wherein rotor, including said blades, had a mass of less than 40 grams.

20 13. The ventilator of Claim 7 wherein said rotor further comprises:

25 the convex rotor hub having a central transverse motor shaft receiving aperture formed therein, to facilitate rotation of said rotor by said motor.

14. The ventilator of Claim 7 wherein said rotor is formed of molded material.

15. The ventilator of Claim 7 wherein said blades are formed of aluminum.

30 16. The ventilator of Claim 7 wherein approximately 30-40 blades are positioned on either side of said rotor.

17. The ventilator of Claim 1 further comprising: a differential pressure transducer for measuring the difference in pressure between gas entering the inlet of 35 said compressor and gas exiting the outlet of said compressor.

18. The ventilator of Claim 1 further comprising:

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a tachometer for measuring the rotational speed of said compressor.

19. The ventilator of Claim 18 wherein said tachometer comprises an optical encoder.

5 20. The ventilator of Claim 1 further comprising: a differential pressure transducer for measuring the difference in pressure between gas entering the inlet of said compressor and gas entering the outlet of said compressor;

10 a tachometer for measuring the rotational speed of said compressor; and

 said differential pressure transducer and said tachometer being in communication with said controller; and

15 said controller being programmed to determine the instantaneous flow rate and current accumulated volume of inspiratory gas flow delivered by said ventilator based on the pressure differential measured by said differential pressure transducer and the rotational speed
20 measured by said tachometer.

21. The ventilator of Claim 1 wherein said compressor incorporates a controller-readable data base containing specific rotational speed, differential pressure and flow rate data for that particular
25 compressor; and

 wherein said controller is further programmed to read said data base and to utilize information obtained from said data base in the calculation of inspiratory flow, volume or pressure delivered by
30 said ventilator.

22. The ventilator of Claim 21 wherein said controller-readable data base comprises an EPROM.

23. The ventilator of Claim 1 further in combination with a portable battery for supplying power
35 to said device.

24. The ventilator of Claim 23 wherein said portable battery contains sufficient power to operate

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said mechanical ventilator device for at least two hours.

25. A drag compressor apparatus for creating inspiratory gas flow in a mechanical ventilator, said compressor apparatus comprising:

5 a housing having a gas inflow passageway and a gas outflow passageway;

10 a rotor rotatably mounted within said housing, said rotor being configured and constructed such that rotation of said rotor in a first direction will cause said rotor to a) draw gas in said inflow passageway, b) compress said gas and c) expel said gas out of said outflow passageway;

15 a controller for controlling the rotation of said rotor within said housing, said controller being operative to cause said rotor to intermittently accelerate and decelerate so as to deliver discrete periods of inspiratory gas flow through said outflow passageway.

20 26. The compressor of Claim 25 wherein said rotor incorporates at least one series of blades having leading edges, each of said blades being disposed at a positive angle of attack such that, when said rotor is rotated in said first direction, the leading edge of each blade will precede the remainder thereof.

25 27. The compressor of Claim 26 wherein said blades are disposed at angles of attack of 30-60 degrees.

28. The compressor of Claim 27 wherein said blades are disposed at 55 degree angles of attack.

30 29. The compressor of Claim 26 wherein said blades are disposed at spaced intervals within an annular trough which extends about said rotor such that, when said rotor is rotating said first direction, said blades will serially contact and compress gas within said housing.

35 30. The compressor of Claim 29 wherein said housing is further configured to define therewithin at least one compressor flow path said flow path being positioned in relation to said annular trough and being connected to

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said inflow and outflow passageways such that, when said rotor is rotated in said first direction, the blades of said rotor will a) draw gas inwardly through said inflow passageway into said compressor flow path, b) compress 5 said gas within said compressor flow path, and c) expel said gas out of said outflow passageway.

31. The compressor of Claim 31 wherein each of said blades has a leading edge and at least one peripheral edge, and wherein said blades are mounted within said 10 trough such that the leading edges of the blades extend transversely across the trough and the peripheral edge of said blades are in abutment with said trough.

32. The compressor of Claim 30 wherein said at least one concave annular trough comprises:

15 a first annular trough which extends about the periphery of said rotor on a first side thereof; and,
a second annular trough which extends about the periphery of said rotor on a second side thereof.

33. The compressor of Claim 32 wherein said 20 housing is configured to define therewithin:

a first compressor flow path which is at least partially within said first annular trough and is connected to said inflow passageway and said outflow passageway; and,

25 a second compressor flow path which is at least partially within said second annular trough and is connected to said inflow passageway and said outflow passageway;

30 said first and second compressor flow paths being configured and positioned such that, when said rotor is rotated in said first direction, the blades mounted within said first annular trough will draw gas into said inflow passageway, compress said gas within said first flow path, and expel said gas out of said outflow passageway and the blades mounted 35 within said second annular trough will draw gas into said inflow passageway, compress said gas within said

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second flow path, and expel said gas out of said outflow passageway.

34. The compressor of Claim 33 wherein said first concave trough and the blades mounted therewithin are 5 mirror images of said second concave trough and the blades mounted therewithin.

35. The compressor of Claim 25 further comprising a drive motor located within said compressor housing and coupled to said rotor to rotatably drive said rotor.

10 36. The compressor of Claim 25 wherein said housing further comprises a number of heat dissipation fins formed on the outside of the portion of said housing wherein said motor is positioned to facilitate dissipation of heat from said motor.

15 37. The compressor of Claim 35 further comprising a tachometer for measuring the rotational speed of said rotor.

38. The compressor of Claim 37 wherein said tachometer comprises an optical encoder.

20 39. The compressor of Claim 25 further comprising: a differential pressure transducer for measuring the difference between the pressure of gas in said inflow passageway and the pressure of gas in said outflow passageway.

25 40. An exhalation valve for controlling the expiratory gas flow from a mammalian patient, said exhalation valve comprising:

a housing defining an expiratory gas flow passageway therethrough;

30 a valve seat formed within said expiratory gas flow passageway;

an annular diaphragm movably disposed within said gas flow passageway, in juxtaposition to said valve seat, said diaphragm being variably movable back and forth to various positions between and including:

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- i) a fully closed position wherein said diaphragm is firmly seated against said valve seat to prevent gas from flowing through said passageway; and
- 5 ii) a fully open position wherein said diaphragm is retracted away from said annular valve seat so as to permit substantially unrestricted flow of expiratory gas through said pathway;
- 10 an elongate actuation shaft having a proximal end and a distal end, the distal end of said actuation shaft being contactable with said diaphragm, and said actuation shaft being axially moveable back and forth to control the positioning of said diaphragm between said fully closed and said fully open positions;
- 15 an electrical induction coil linked to said actuation shaft such that a decrease in the current passing into said induction coil will cause said shaft to advance in the distal direction and an increase in the current passing into said induction coil will cause said shaft to retract in the proximal direction;
- 20 means for determining the flow rate of expiratory gas passing out of said exhalation valve;
- 25 means for determining airway pressure;
- 30 a microprocessor controller connected to said means for determining airway pressure, said controller being provided with a positive expiratory pressure setting, and said controller being connected to said induction coil and adapted to emit control signals to said induction coil to control the movement of said actuation shaft in response to the current airway pressure, thereby maintaining the present amount of positive expiratory pressure;
- 35 a radio frequency transponder database containing flow characterization data for the means

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for determining the flow rate of expiratory gas passing out of said exhalation valve;

said controller being further connected to said means for determining the flow rate of expiratory gas passing out of said exhalation valve and being equipped to receive radio frequency input of the characterization data contained in the radio frequency transponder database, and to utilize such data to determine the instant flow rate of expiratory gas passing out of said exhalation valve.

5 41. The exhalation valve of Claim 40 wherein said controller is located separately from, said exhalation valve.

10 42. The exhalation valve of Claim 40 wherein said controller is further adapted to receive input signals from said means for determining the flow rate at which expiratory gas is passing outwardly through said expiratory gas flow passageway, and for emitting control signals to said induction coil to fully close said diaphragm when said flow rate has fallen to a predetermined basal level, thus signifying the end of the expiratory phase.

15 43. A method of providing pulmonary ventilation to a mammalian patient, said method comprising the steps of:

20 25 a) providing a rotary drag compressor device comprising:

i) a housing having an inflow passageway and an outflow passageway formed therein; and,

30 ii) a rotor rotatably mounted within said housing such that rotation of said rotor in a first direction will draw gas into said inflow passageway, compress said gas, and expel said gas out of said outflow passageway;

35 b) connecting the outflow passageway of said rotary drag compressor to a conduit through which respiratory gas flow may be passed into the patient's lungs;

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c) accelerating said rotor to a first rotational speed for sufficient time to deliver a desired inspiratory gas flow through said conduit and into the patient's lungs;

5 d) stopping said rotor or decelerating said rotor to a basal rotational speed to terminate the inspiratory gas flow through said conduit and to allow the expiratory phase of the ventilation cycle to occur.

10 44. The method of Claim 43 wherein step b comprises connecting said outflow passageway to an endotracheal tube inserted into the trachea of the patient.

15 45. The method of Claim 43 wherein step b comprises connecting said outflow passageway to a nasotracheal tube inserted into the trachea of the patient.

46. The method of Claim 43 wherein step b comprises connecting said outflow passageway to a tracheostomy tube inserted into the trachea of the patient.

20 47. The method of Claim 43 wherein step b comprises connecting said outflow passageway to a mask which is positioned over the nose and mouth of the patient.

48. The method of Claim 43 wherein step c is commenced upon the occurrence of a triggering event, said triggering event being selected from the group of 25 triggering events consisting of:

i) the passing of a predetermined time period; and

ii) the initiation of spontaneous inspiratory effort by the patient.

30 49. The method of Claim 43 wherein the inspiratory gas flow delivered in step c is limited by a limiting parameter selected from the group of limiting parameters consisting of:

i. a predetermined minimum airway pressure;
35 ii. a predetermined maximum airway pressure;
iii. a predetermined minimum flow rate;
iv. a predetermined maximum flow rate;

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- v. a predetermined minimum tidal volume; and
- vi. a predetermined maximum tidal volume.

50. The method of Claim 43 wherein step c is terminated and step d is commenced upon the occurrence of
5 a selected terminating event, said terminating event being selected from the group of terminating events consisting of:

- i. the passing of a predetermined period of time since the commencement of step c;
- 10 ii. the attainment of a predetermined airway pressure; and
- iii. the passage of a predetermined tidal volume of inspiratory gas.

51. The method of Claim 43 wherein step c further comprises controlling the speed to which said rotor is accelerated during the inspiratory phase by:

- i. storing specific rotor speed, compressor differential pressure and flow rate characterization data for the compressor;

20 ii. providing a first input signal to said compressor which is intended to cause the rotor to rotate at a speed calculated to deliver a desired flow rate;

25 iii. determining the actual flow rate generated by said compressor in response to said first input signal;

iv. comparing the actual flow rate determined in step iii, to the desired flow rate;

30 v. adjusting the input signal to said compressor to provide the desired flow rate.

52. The method of claim 51 wherein step c further comprises:

vi. repeating steps ii-v, as necessary to achieve said desired flow rate.

35 53. A rotary drag compressor ventilator device for delivering inspiratory gas flow to a mammalian patient, said device comprising:

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- a) a rotary drag compressor having an intake port and an outflow port;
- 5 b) an inspiratory gas flow passageway for carrying gas from the outflow port of the compressor to the patient during the inspiratory phase of the ventilation cycle;
- 10 c) means for accelerating said compressor at the beginning of the inspiratory phase of the ventilation cycle to deliver inspiratory gas flow through said passageway to said patient;
- d) means for controlling said compressor during the inspiratory phase of the ventilation cycle to maintain a desired inspiratory pressure and flow rate; and,
- 15 e) means for decelerating said compressor at the end of the inspiratory phase of the ventilation cycle.
54. The ventilator device of Claim 53 wherein said inspiratory gas flow passageway is devoid of valves for diverting the inspiratory gas flow away from said patient.
- 20 55. The ventilator device of Claim 53 wherein said rotary drag compressor comprises:
- 25 a compressor housing having said intake and outflow ports formed therein;
- 30 a rotor mounted within said housing such that rotation of said rotor in a first direction will cause said inspiratory gas flow to be delivered out of said outflow port and through said inspiratory gas flow passageway to said patient; and,
- 35 a motor for rotating said rotor within said housing.
56. The ventilator device of Claim 53 wherein said means for accelerating, controlling and decelerating said compressor comprise:
- a microprocessor controller connected to said compressor.

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57. The ventilator device of Claim 53 further comprising:

5 f) an exhalation conduit for carrying expiratory gas flow from said patient during the expiratory phase of the ventilation cycle;

10 g) an exhalation valve positioned on said exhalation conduit, said exhalation valve being constructed to:

15 i) open during the expiratory phase of the ventilation cycle to permit the expiratory gas flow to pass out of said exhalation conduit, and

15 ii) close during the inspiratory phase of the ventilation cycle to prevent gas from being drawn into said patient through said exhalation conduit.

58. The ventilator device of Claim 53 further comprising:

20 f) an oxygen blending apparatus connected to said intake port to provide oxygen-enriched air to said compressor.

59. An exhalation valve comprising:

25 a) a housing defining a first exhalation passageway through which expiratory gas may outflow in a first direction;

b) a valve seat formed within said passageway;

30 c) a diaphragm having a front side and a back side, said diaphragm being sized and configured such that the front side thereof may abut against said valve seat to thereby block the flow of gas through said exhalation passageway, said diaphragm being moveable back and forth between;

35 i) a first position wherein said diaphragm is fully retracted from said valve seat to permit unrestricted flow through said passageway;

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- ii) a second position wherein said diaphragm is seated on said valve seat to block flow through said passageway;
- iii) a range of intermediate positions between said first and second positions wherein said diaphragm will cause varying degrees of restriction of the flow through said passageway;
- d) an elongate shaft having a first end and a second end, the first end of said shaft being adjacent to the back side of said diaphragm, said shaft being axially moveable back and forth between;
- i) a first position wherein the first end of said shaft is at a location which will retain said diaphragm in its first position;
- ii) a second position wherein the first end of said shaft is at a location which will allow said diaphragm to move to its second position; and,
- iii) a range of intermediate positions wherein said shaft is at a location which will allow said diaphragm to move to one of its intermediate positions;
- e) an electrical induction coil slidably mounted within said housing so as to move back and forth in response to changes in current applied to the coil, said coil consisting essentially of multiple convolutions of wire upon which a rigidifying coating has been applied to hold said wire in a closely coiled substantially cylindrical configuration;
- f) a mounting spider connecting said shaft to said coil, said spider configured to hold said shaft in co-axial alignment with the longitudinal axis of the coil, with the first end of the shaft protruding toward the back side of said diaphragm such that, when the coil moves forward, said shaft will move

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forward toward said first shaft position, and when said coil moves rearward, said shaft will be retracted toward said second shaft position.

60. The exhalation valve of Claim 59 wherein the
5 front surface of said diaphragm is planar and wherein
said valve seat is angled relative to the plane of the
front surface of the diaphragm such that, when said
diaphragm is moving into said first diaphragm position,
the front side of said diaphragm will initially contact
10 only one side of said diaphragm and will subsequently
move into contact with the remainder of said valve seat.

61. The exhalation valve of Claim 59 further
comprising:

15 g) a pliable dust barrier disposed between
said valve seat and said induction coil, said
pliable dust barrier being sealed to the surrounding
housing to prevent particulate matter from passing
around said shaft and into said induction coil, said
dust barrier being in contact with said shaft and
20 being sufficiently flexible to move back and forth
in accordance with axial movement of said shaft.

62. The exhalation valve of Claim 61 wherein said
dust barrier comprises an elastomeric boot.

63. The exhalation valve of claim 61 wherein at
25 least one vent hole is formed in said exhalation valve to
prevent the creation of pressure on at least one side of
said dust barrier as said dust barrier flexes back and
forth.

64. An exhalation valve comprising:
30 a) a housing defining an expiratory gas flow
path connectable to a mammalian patient such that
expiratory gas exhaled by the patient will pass
through said flow path in a first direction;

35 b) a valve associated with said flow path to
permit gas exhaled by the patient to pass through
said flow path in said first direction, but to
prevent gas from being drawn through said flow path,

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in a second direction opposite said first direction, when said patient inhales;

5 c) a flow measuring apparatus for monitoring the flow rate of expiratory gas passing through said exhalation valve.

65. The exhalation valve of Claim 64 wherein said flow measuring apparatus comprises:

10 a flapper disposed transversely within said flow path, said flapper being constructed such that at least a portion of said flapper will deflect in a first direction when exhaled gas is passed through said flow path in said first direction, the extent of flapper deflection being variable with the flow rate of gas passing through the exhalation valve, 15 said flapper thereby creating a dynamic flow restricting orifice within said flow path;

means for determining gas pressure within said flow path upstream of said flapper;

20 means for determining gas pressure within said flow path downstream of said flapper; and

means for determining the then-current flow rate of gas passing through said exhalation valve, based on the difference in the pressures measured upstream and downstream of said flapper.

25 66. The exhalation valve device of Claim 65 wherein said flapper is mounted within a flapper assembly which comprises:

30 a sheet of pliable material having a first side, a second side and an outer peripheral edge, a semi-annular cut being formed in said sheet to divide said sheet into i) an outer peripheral portion which is outboard of said cut and ii) an inner flapper portion which is inboard of said cut, and which remains attached on one side thereof to the surrounding peripheral portion of said sheet, 35 said inner flapper portion of said sheet being thereby deflectable back and forth while the outer

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peripheral portion of said sheet is held in substantially stationary position;

5 a first frame member having a central aperture formed therein, said first frame member being juxtaposed to the first side of said sheet such that said first frame member is in contact with the first side of the peripheral portion of said sheet such that said first frame member is in abutment with the first side of the peripheral portion of said sheet and the central aperture of said first frame member surrounds the first side of the flapper portion of said sheet;

10 a second frame member having a central aperture formed therein, said second frame member being juxtaposed to the second side of said sheet such that said frame member abuts against the second side of the peripheral portion of said sheet, and the central aperture of said second frame member surrounds the second side of the flapper portion of said sheet;

15 said first and second frame members thereby holding the peripheral portion of said sheet in a substantially fixed position between said frame members while the flapper portion of said sheet extends transversely into the space between the axially aligned apertures of said frame members and is deflectable back and forth therein.

20 67. The exhalation valve device of Claim 66 wherein said flapper assembly is positioned transversely within the flow path of said exhalation valve and is held in such position by engagement to the surrounding exhalation valve housing.

25 68. The exhalation valve device of Claim 64 further comprising:

30 specific flow-pressure calibration information for the flow measuring apparatus stored on a storage

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medium contained within the exhalation valve housing.

69. The exhalation valve device of Claim 68 wherein said storage medium comprises a radio-frequency 5 transponder.

70. The exhalation valve device of Claim 68 wherein the characterization information stored on said storage medium comprises a data base of predetermined pressure differences for specific flow rates of exhalation valve.

10 71. The exhalation valve device of Claim 68 wherein the information stored on said storage medium comprises an equation for calculating specific flow rates based on measured pressure differentials for that exhalation valve.

15 72. The exhalation valve device of Claim 66 further comprising:

20 a cushioning washer and a third frame member disposed on at least one of the first and second frame members which abut against the same so as to evenly distribute stresses applied to said sheet by said frame members.

73. The exhalation valve device of Claim 72 wherein said cushioning washer comprises an elastomeric material disposed on said third frame member.

25 74. An oxygen blending apparatus for delivering oxygen enriched air to a ventilator, said apparatus comprising:

- a) an accumulator chamber;
- b) an air inlet conduit connected to said 30 accumulator chamber;
- c) an oxygen inlet conduit connected to said accumulator chamber;
- d) a series of solenoid valves connected, in parallel, within said oxygen inlet conduit, each of 35 said solenoid valves having a predetermined orifice size; and

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e) a controller for independently opening and closing each of the solenoid valves to control the amount of oxygen which flows into the accumulator chamber during a time period.

5 75. The oxygen blending apparatus of Claim 74 further in combination with a ventilator device connected to the outlet of said accumulator chamber, said ventilator device being operative to intermittently draw inspiratory gas from said accumulator chamber to compress
10 and expel said gas to provide an inspiratory flow.

76. The oxygen blending apparatus of Claim 75 wherein said controller is further programmed to repeatedly determine the volume of oxygen enriched gas which has been drawn from the accumulator chamber during
15 the then-current inspiratory phase, and to subsequently adjust the opening and closing of the solenoid valves to maintain the prescribed oxygen concentration of gas drawn from the accumulator chamber during the remainder of that inspiratory phase.

20 77. The oxygen blending apparatus of Claim 76 wherein said controller is further programmed to repeatedly compare the then-current accumulated volume of oxygen enriched gas to a predetermined trigger volume for each of the solenoid valves, and to open each solenoid
25 valve for a predetermined period of time when it is determined that the accumulated volume of oxygen-enriched air has exceeded the trigger volume for that individual solenoid valve.

78. The oxygen blending apparatus of Claim 74
30 wherein said solenoid valves comprise at least first, second, third and fourth solenoid valves, and wherein a predetermined oxygen pressure is constantly passed into said oxygen inlet conduit.

79. The oxygen blending apparatus of Claim 78
35 wherein said first, second, third, and fourth solenoid valves have flow rates, at a predetermined oxygen inlet operating pressure, of 5 liters/min., 14.7

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liters/min.; 40 liters/min. and 80 liters/min., respectively.

80. A flow transducer for measuring the flow rate of a fluid, said transducer comprising:

5 a housing defining a first fluid flow path therethrough;

10 a deflectable flapper disposed transversely within said fluid flow path such that said flapper will deflect in the direction of fluid flow, thereby creating a fluid flow restriction permitting some fluid to flow past said flapper and through said flow path;

15 a first pressure port located upstream of said flapper for measuring the pressure of fluid within said flow path, upstream of said flapper;

a second pressure port downstream of said flapper for measuring the pressure of fluid flowing through said flow path, downstream of said flapper;

20 means associated with first pressure port for determining the pressure of fluid flowing upstream of said flapper;

means associated with said second pressure port for determining the pressure of fluid flowing downstream of said flapper;

25 means for determining the difference between the pressure of fluid flowing upstream of said flapper and the pressure of fluid flowing downstream of said flapper, and

30 means for computing the flow rate of fluid through said flow path, based on the measured difference in pressures upstream and downstream of said flapper.

81. The fluid flow transducer of Claim 80, wherein said deflectable flapper comprises:

35 a rigid frame having a central aperture formed therein;

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5 a flat sheet of pliable material mounted within said frame member and forming a flapper disposed transversely within the central aperture of said frame and deflectable in at least one direction to permit fluid to flow past said flapper and through said central aperture;

10 said frame being mounted transversely within said flow path such that fluid flowing in a first direction through said flow path will strike said flapper, thereby causing said flapper to deflect in the direction of flow such that the flowing fluid may pass through said central aperture.

82. The flow transducer of Claim 81 wherein:

15 said flat sheet of pliable material comprises an outer peripheral portion, an inner flapper portion, and a semi-annular cut formed in said sheet to free most of said peripheral portion from said flapper portion; and

20 said rigid frame comprises first and second frame members disposed on opposite sides of the peripheral portion of said flat sheet, said frame members being compressed inwardly to compressively hold said peripheral portion of said flat sheet between said frame members such that the flapper portion of said flat sheet is transversely disposed and deflectable within the central aperture of said frame.

25 83. The flow transducer of Claim 80 further comprising:

30 35 a cushioning member associated with said flapper to distribute the force exerted on said flapper thereby distributing any stresses created within said flapper.

84. The flow transducer of Claim 81 further comprising:

 a cushioning member associated with said frame to distribute the force exerted by said frame on

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said flat sheet of pliable material, thereby distributing any stresses of created within said flat sheet of pliable material.

85. The flow transducer of Claim 80 wherein said 5 housing comprises a portion of an exhalation valve through which a mammalian patient is permitted to exhale, said flow transducer being disposed within said exhalation valve to measure the flow rate of expiratory gas passing through said exhalation valve.

10 86. The flow transducer of Claim 80 further comprising:

15 a deflector member positioned on at least one of said first and second pressure ports to deter fluid from being forced directly into the pressure port on which deflector insert is positioned.

87. The flow transducer of Claim 80 wherein said means for computing flow rate comprises a microprocessor.

88. The flow transducer of Claim 82 wherein:

20 said housing incorporates first and second abutment ridges formed about said flow path;

25 said first and second frame members, having said flat sheet of pliable material therebetween, being positioned between said abutment ridges such that said abutment ridges will exert inward compressive force on said first and second frame members to compressively hold said flat sheet therebetween.

89. The flow transducer of Claim 81 further comprising:

30 specific flow-pressure calibration information for the flow transducer stored on a storage medium contained within said housing.

90. The flow transducer of Claim 89 wherein said storage medium comprises a radio-frequency transponder.

35 91. The flow transducer of Claim 89 wherein the specific flow-pressure calibration information stored on said storage medium comprises a data base of

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predetermined pressure differences for specific flow rates of fluid through said flow path.

92. The flow transducer of Claim 89 wherein the calibration information stored on said storage medium
5 comprises an equation for calculating specific flow rates based on measured differences in pressure upstream and downstream of said flapper.

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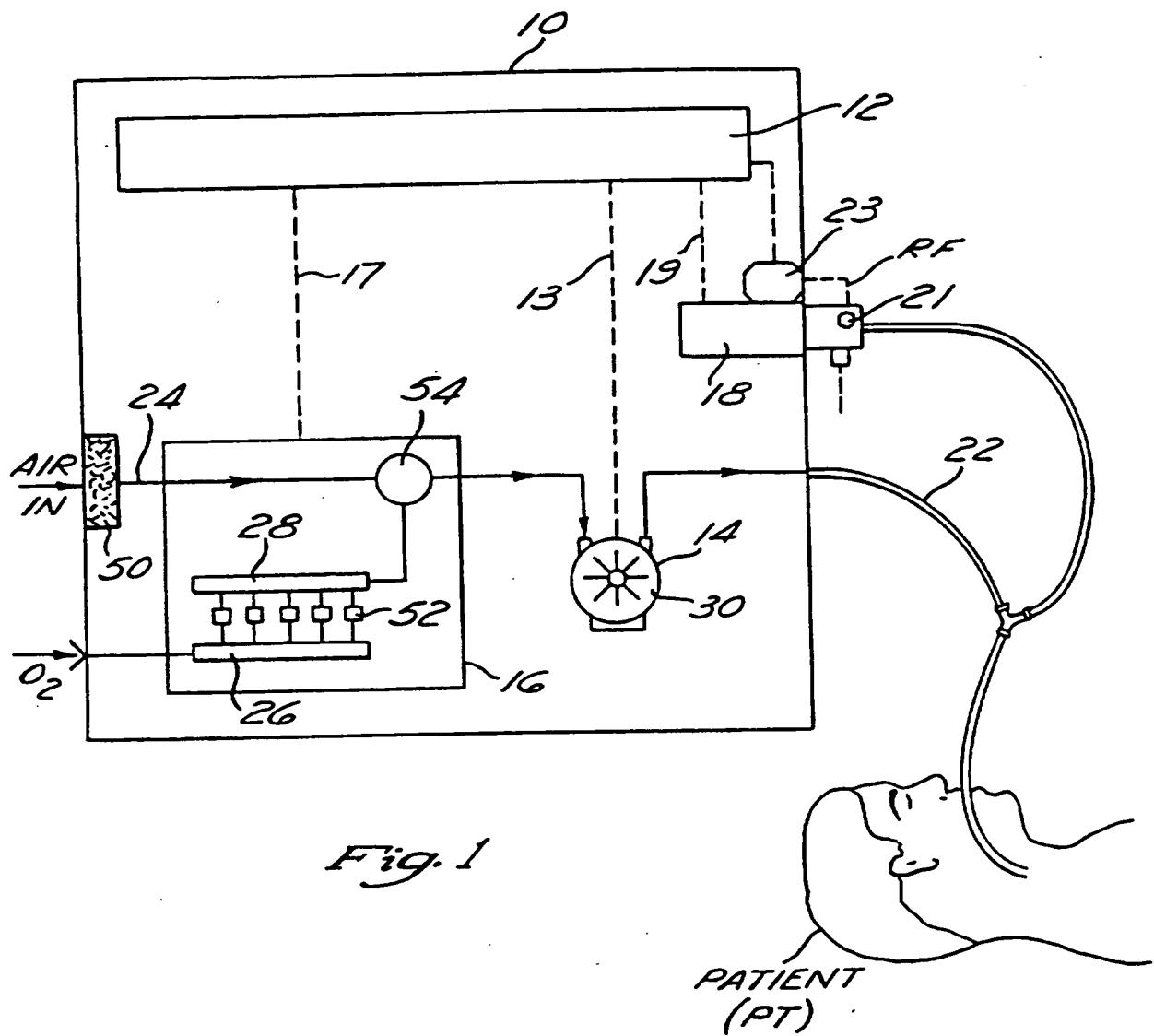


Fig. 1

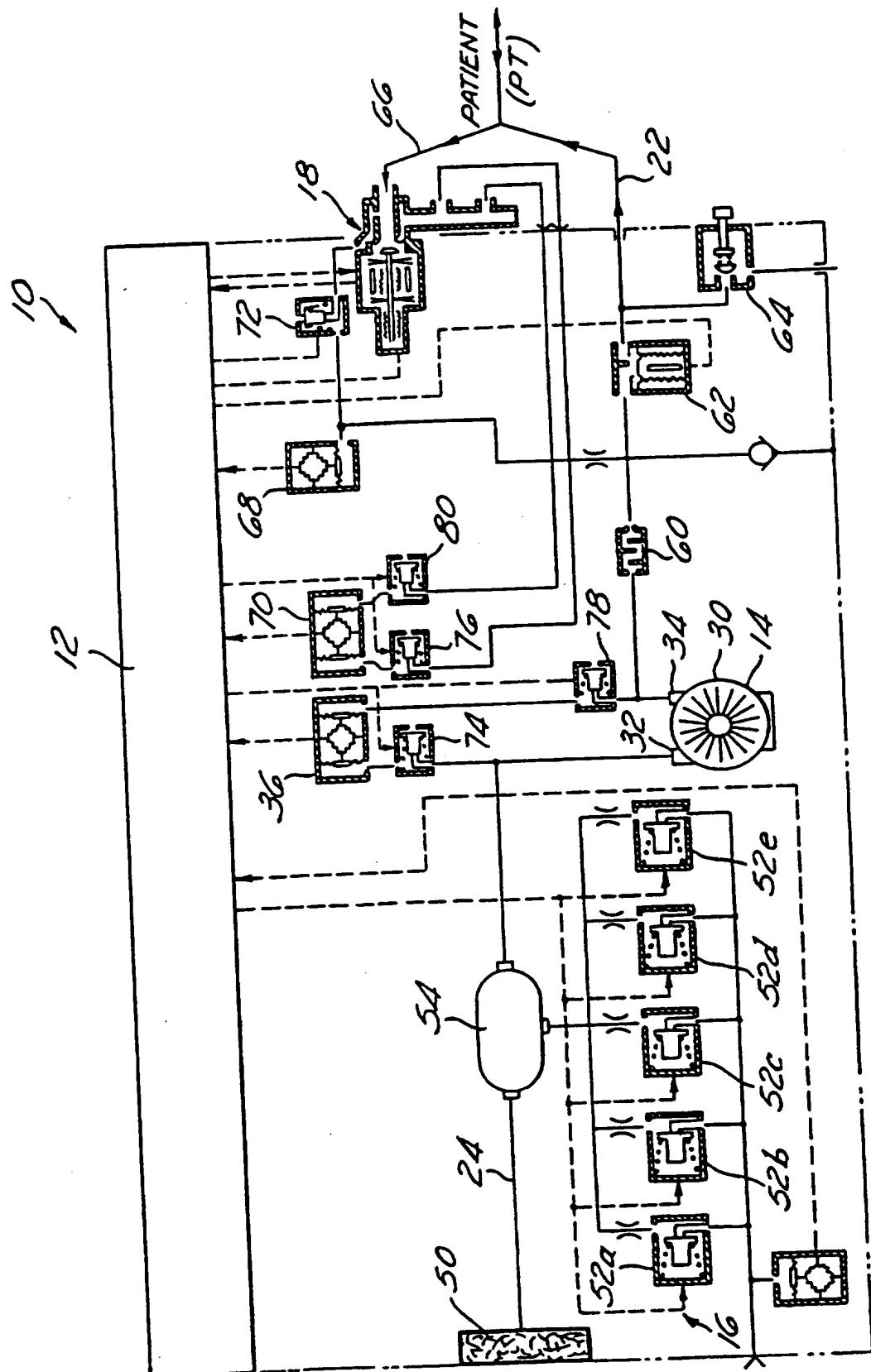
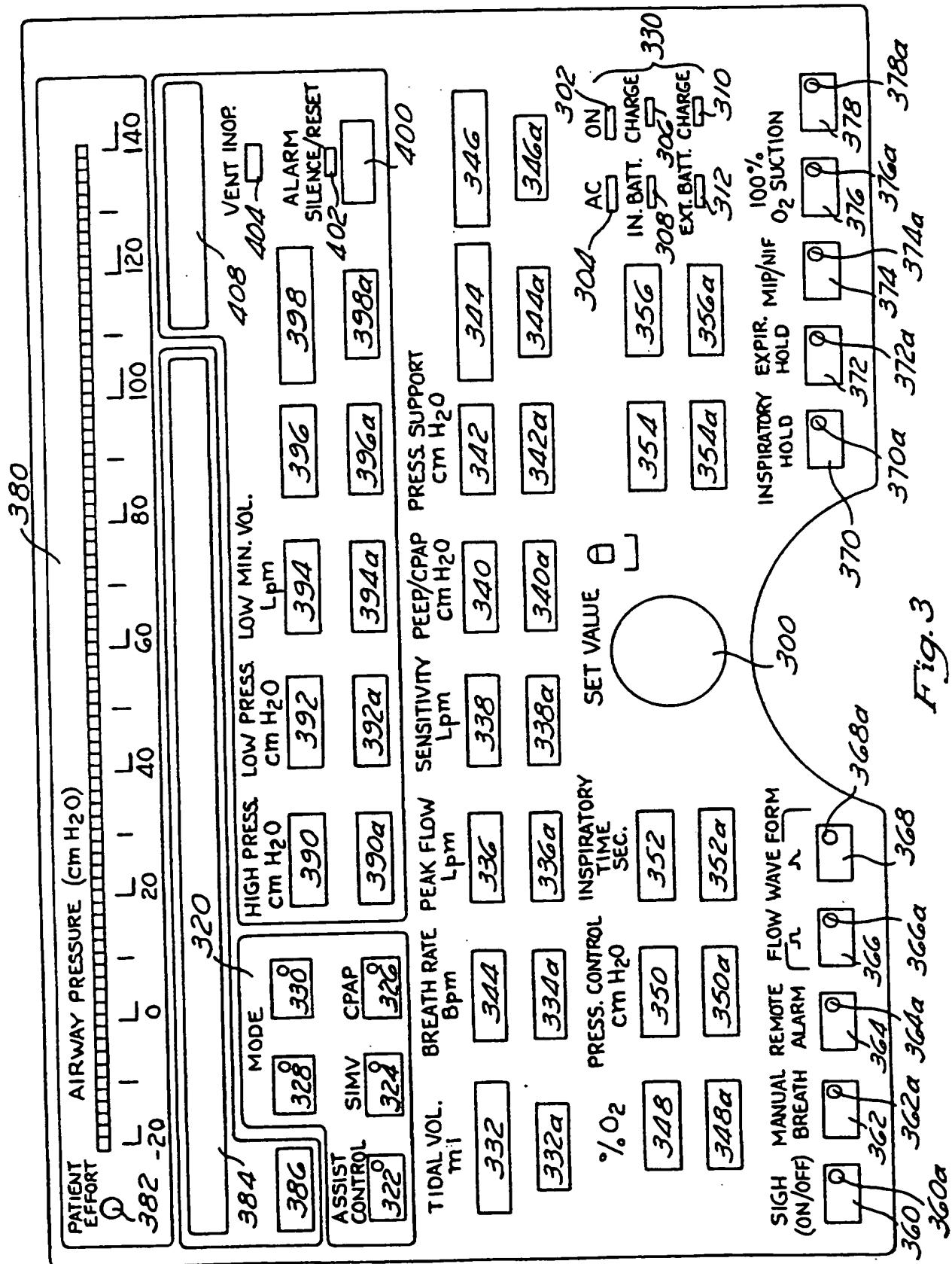
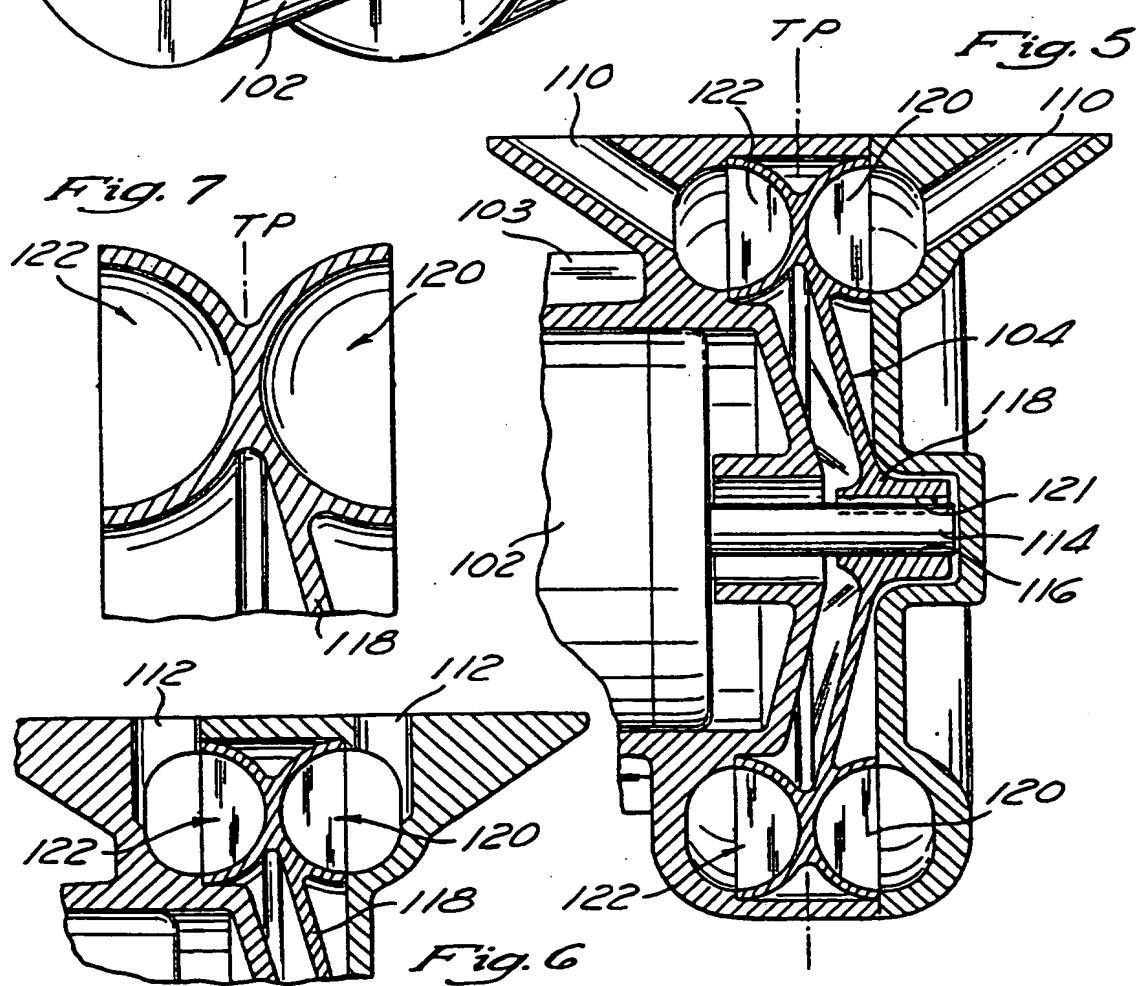
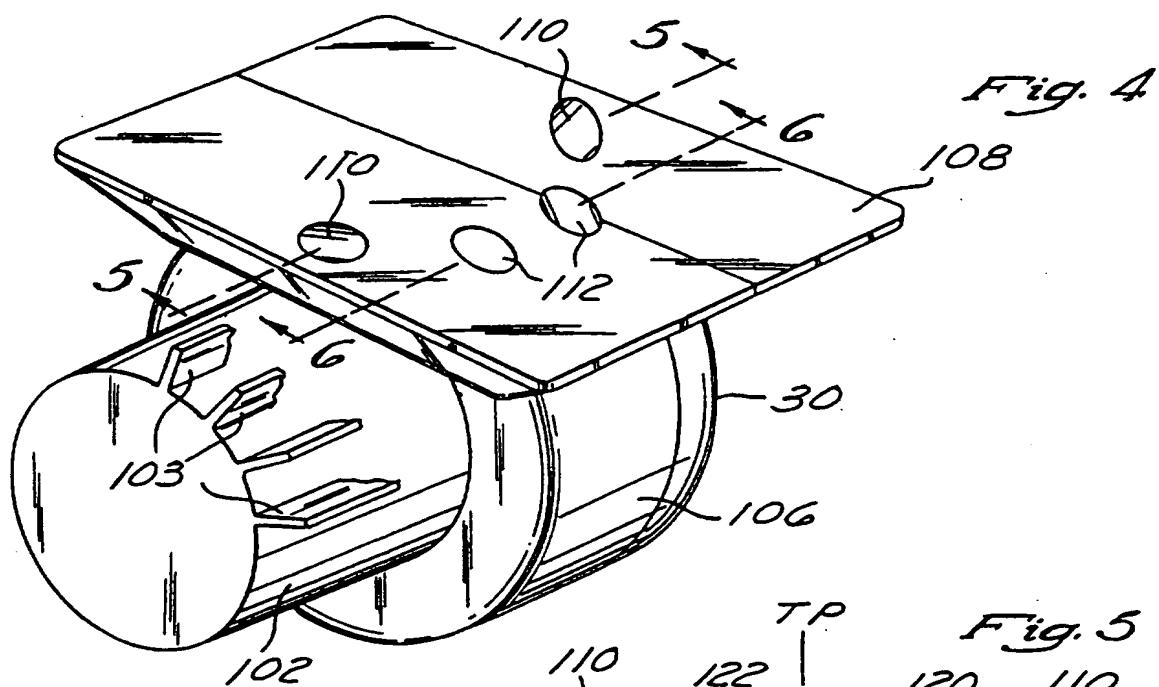


Fig. 2

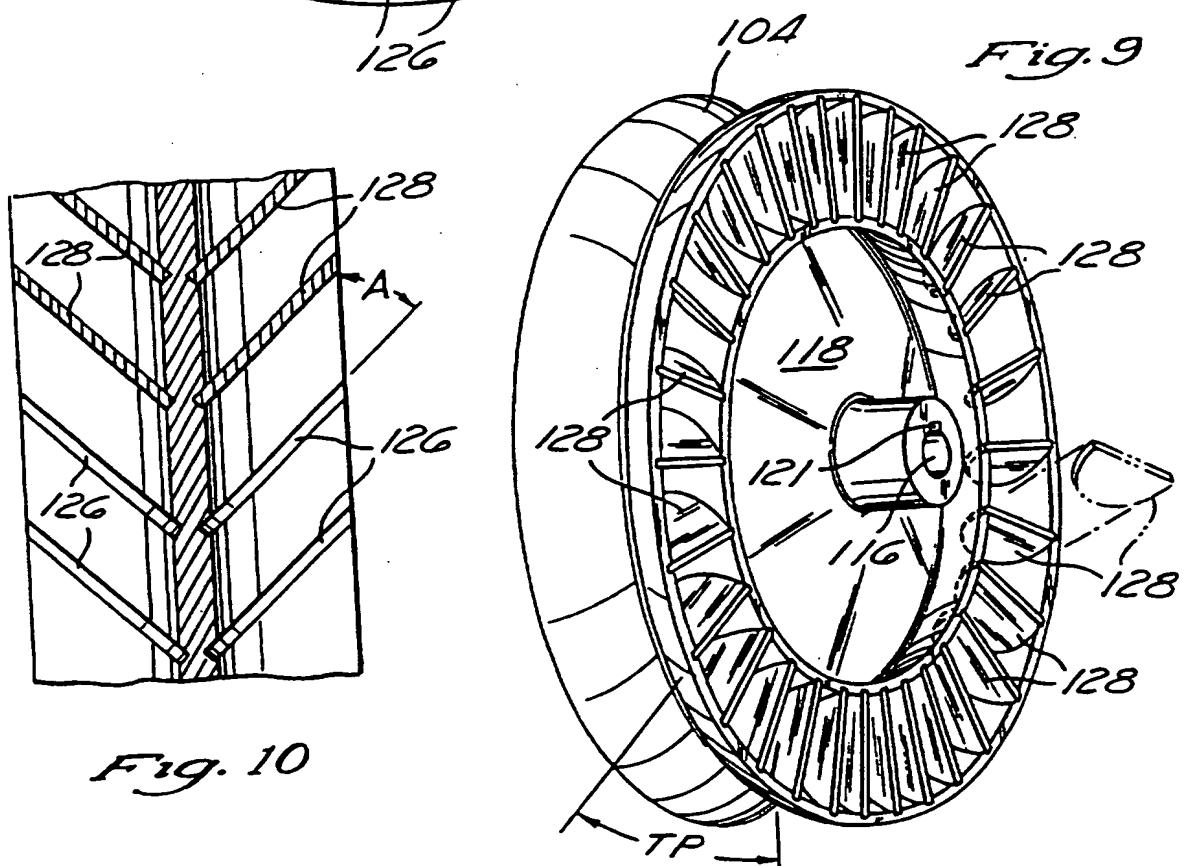
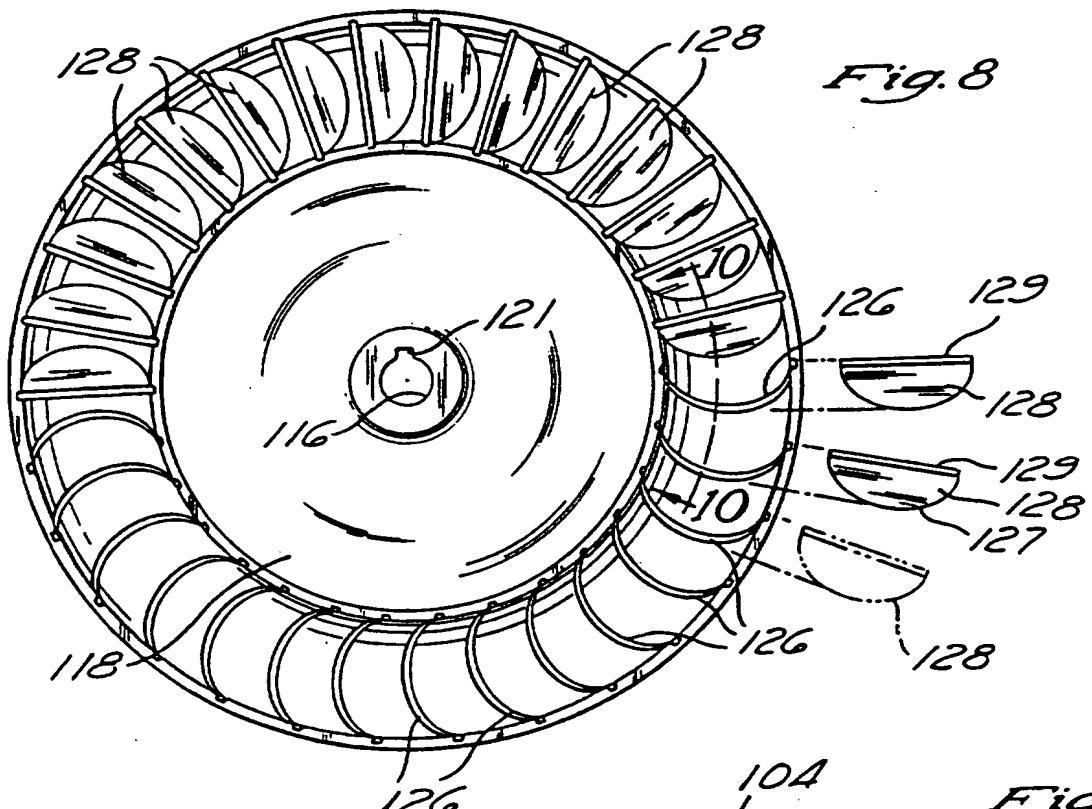
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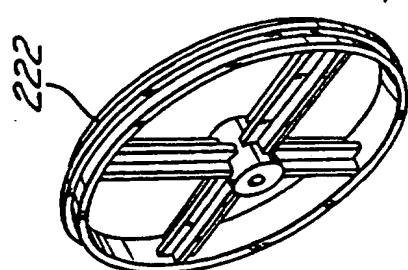
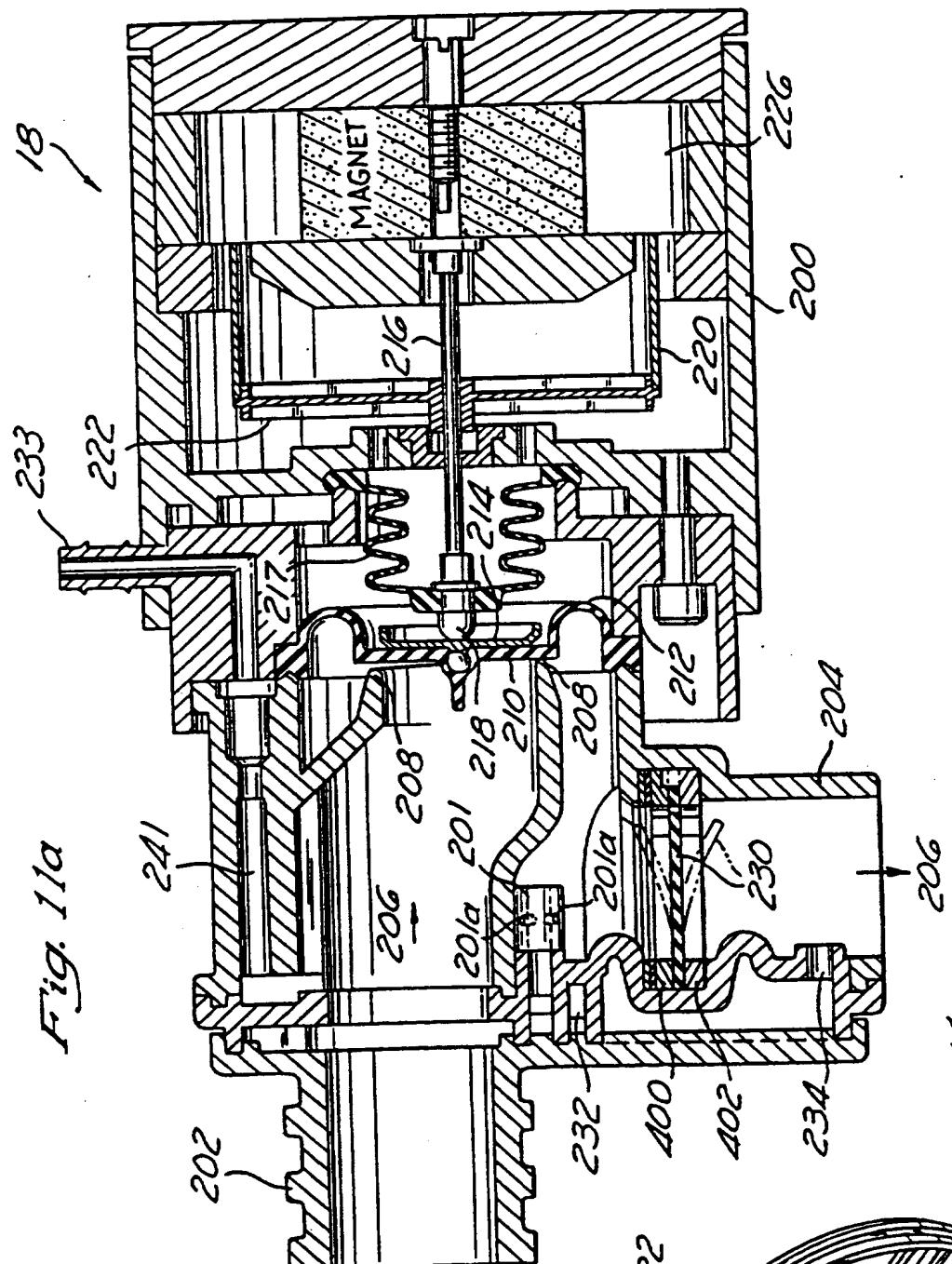
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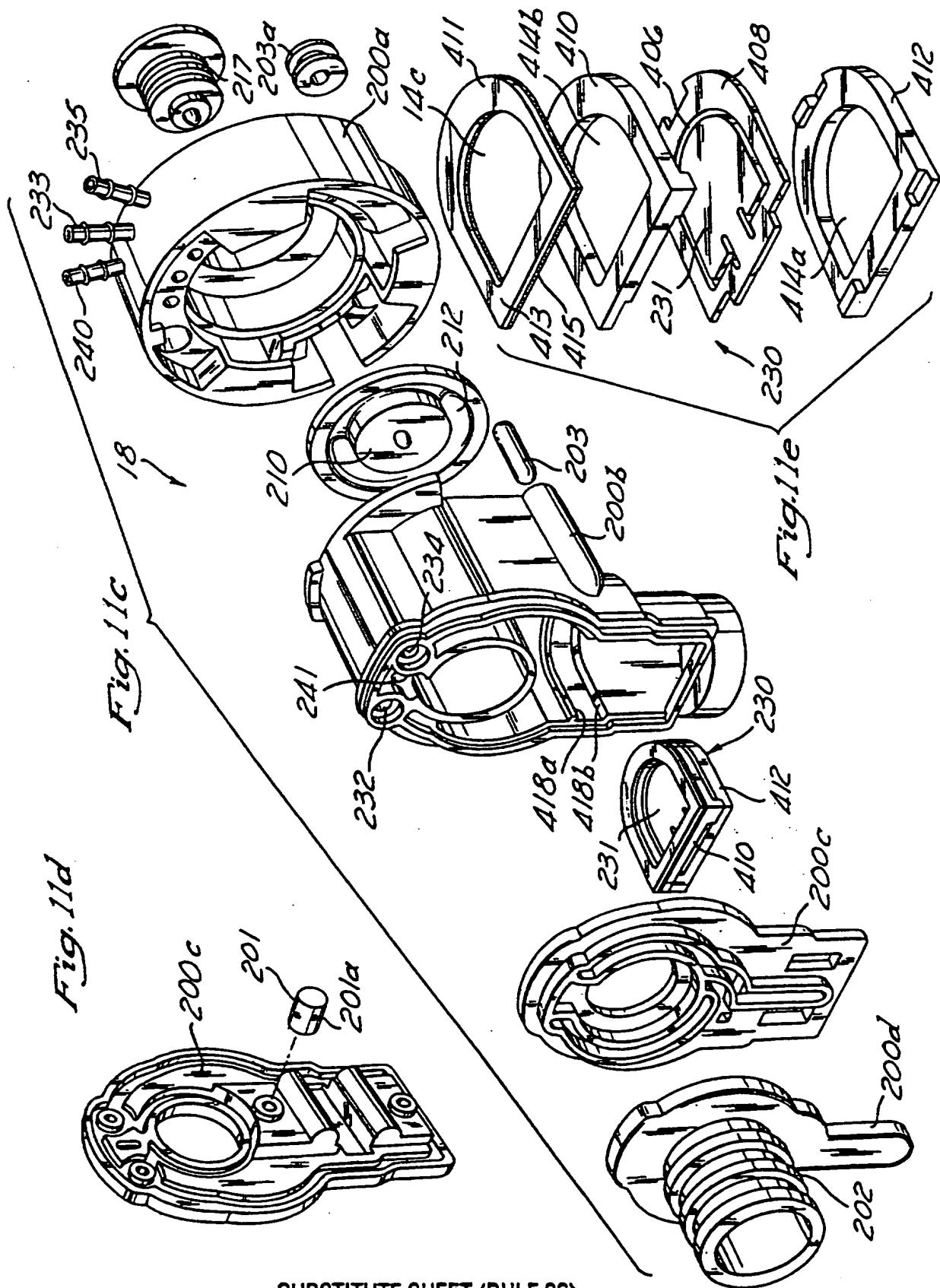
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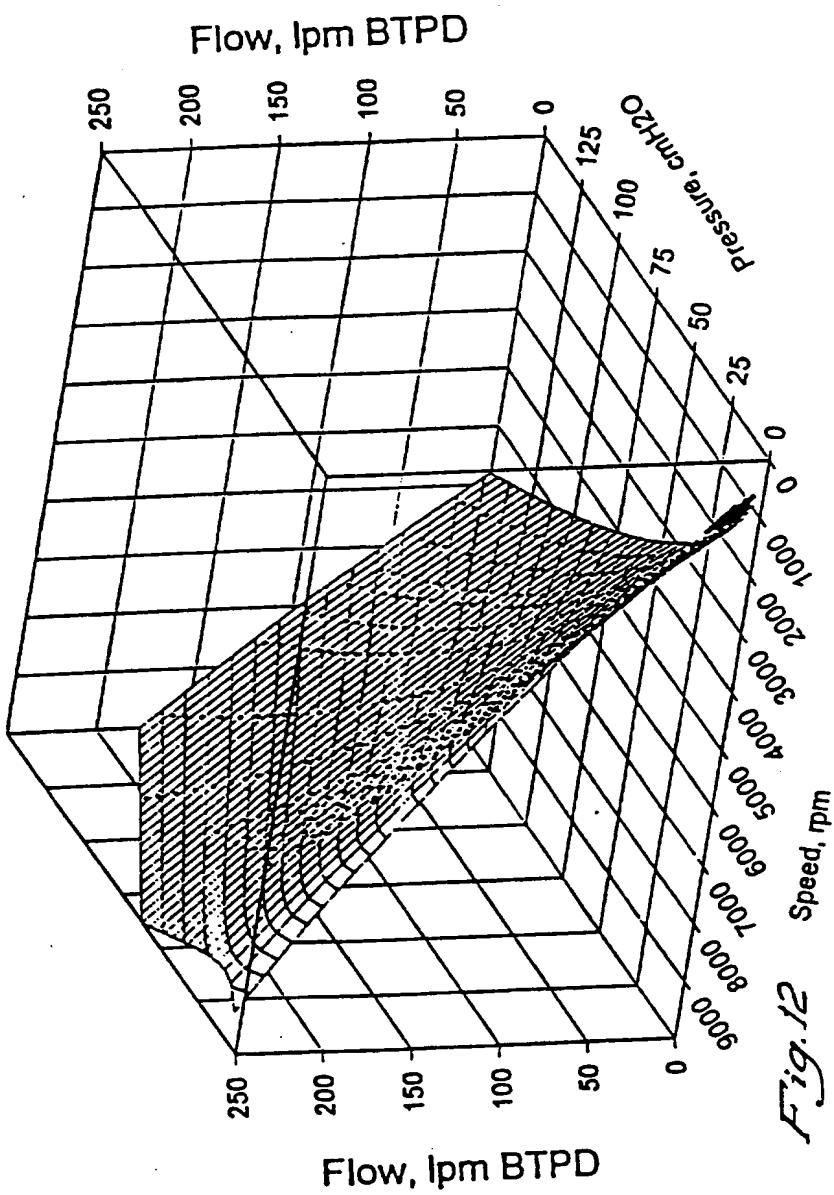
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INTERNATIONAL SEARCH REPORT

International application No.

PCT/US95/08499

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) : A61M 16/00; A62B 7/00; F16K 1/08

US CL : 128/204.23

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : Please See Extra Sheet.

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
noneElectronic data base consulted during the international search (name of data base and, where practicable, search terms used)
Please See Extra Sheet.**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US, A, 5,148,802 (SANDERS ET AL) 22 September 1992.	1-38,40-63, 67-75, 79, 82, 83, 89
Y -- X	US, A, 4,957,107 (SIPIN) 18 September 1990. See entire document.	1-38,40-63, 67-75, 79, 82, 83, 89 ----- 66
Y	US, A, 5,315,990 (MONDRY) 31 May 1994. See entire document.	3-5, 76-78, 80, 81
Y	US, A, 4,617,637 (CHU ET AL) 14 October 1986. See entire document.	18-22, 37, 38

 Further documents are listed in the continuation of Box C.

See patent family annex.

A	Special categories of cited documents:	T	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
E	document defining the general state of the art which is not considered to be part of particular relevance	X	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
L	earlier document published on or after the international filing date	Y	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is taken alone
O	document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reasons (as specified)	Z	document referring to an oral disclosure, use, exhibition or other means
P	document referring to an oral disclosure, use, exhibition or other means		document published prior to the international filing date but later than the priority date claimed

Date of the actual completion of the international search

09 NOVEMBER 1995

Date of mailing of the international search report

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Box PCT
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Facsimile No. (703) 305-3230

Authorized officer


KIMBERLY L. ASHER

Telephone No. (703) 308-0858

INTERNATIONAL SEARCH REPORT

International application No.

PCT/US95/08499

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US, A, 4,993,269 (GUILLAUME ET AL) 18 February 1991. See entire document.	84, 85, 90, 91, 93, 95, 96
--		67- 75
Y	US, A, 4,114,601 (ABELS) 19 September 1978. See entire document.	94, 41-44, 61, 62, 71
A	US, A, 3,840,006 (BUCK ET AL) 08 October 1974. See entire document.	1-38,40-96